



## Review

# Heterogeneous electro-Fenton and photoelectro-Fenton processes: A critical review of fundamental principles and application for water/wastewater treatment



Soliu O. Ganiyu<sup>a,\*</sup>, Minghua Zhou<sup>b</sup>, Carlos A. Martínez-Huitl<sup>a,c,\*</sup>

<sup>a</sup> Laboratório de Electroquímica Ambiental e Aplicada, Instituto de Química, Universidade Federal do Rio Grande do Norte, Lagoa Nova, CEP 59.072-900, RN, Brazil

<sup>b</sup> Key Laboratory of Pollution Process and Environmental Criteria (MOE), Tianjin Key Laboratory of Urban Ecology Environmental Remediation and Pollution Control, College of Environmental Science and Engineering, Nankai University, Tianjin 300350, China

<sup>c</sup> Institut für Organische Chemie, Johannes Gutenberg-Universität Mainz, Duesbergweg 10-14, 55128, Mainz, Germany

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## ABSTRACT

This exhaustive review focuses on the fundamental principles and applications of heterogeneous electrochemical wastewater treatment based on Fenton's chemistry reaction. The elementary equations involved in formation of hydroxyl radical in homogeneous electro-Fenton (EF) and photo electro-Fenton (PEF) processes was presented and the advantages of using insoluble solids as heterogeneous catalyst rather than soluble iron salts (heterogeneous electro-Fenton process) (Hetero-EF) was enumerated. Some of the required features of good heterogeneous catalysts were discussed, followed by the mechanisms of catalytic activation of H<sub>2</sub>O<sub>2</sub> to reactive oxygen species (ROS) especially hydroxyl radical (·OH) by heterogeneous catalyst in Hetero-EF system. Extensive discussion on the two configuration of Hetero-EF system *vis-à-vis* added solid catalysts and functionalized cathodic materials were provided along with summaries of some relevant studies that are available in literature. The solid catalysts and the functionalized cathodic materials that have been utilized in Hetero-EF wastewater treatment were grouped into different classes and brief discussion on their synthesis route were given. Besides, the use of solid catalysts and iron-functionalized cathodic materials in bioelectrochemical system (BES) especially bioelectro-Fenton technology (BEF) using microbial fuel cells (MFCs) with concurrent electricity generation for Hetero-EF treatment of biorefractory organic pollutants was discussed. In the final part, emphasis was made on the challenges and future prospects of the Hetero-EF for wastewater treatment.

## 1. Introduction

Electrochemical advance oxidation processes (EAOPs) based on Fenton's chemistry are among the most widely applied advanced oxidation processes (AOPs) for the removal of persistence organic pollutants (POPs) [1–6]. These eco-friendly techniques possess some exciting

advantages such as high versatility, excellent efficiency, high amenability and environmental compatibility, which distinguish them from other AOPs [5–11]. In general, EAOPs based on Fenton's chemistry utilizes hydroxyl radical (·OH) produce from Fenton's reaction between *in-situ* generated or externally added hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) and Fe<sup>2+</sup> ions (Eq. (1)) for the degradation of POPs. The prominent

**Abbreviations:** 2,4-DCP, 2,4-dichlorophenol; 3D, three dimension; AB, alginate beads; AC, activated carbon; ACF, activated carbon felt; ACS, activated charcoal; AOPs, advanced oxidation processes; APHs, 4-Amino-3-hydroxy-2-p-tolylazonaphthalene-1-sulfonic acid; APN, allophone clay; AQ, anthraquinone; ATR-FTIR, attenuated total reflectance-Fourier transforms Infrared spectroscopy; BDD, boron doped diamond; BEF, bioelectro-Fenton technology; BES, bioelectrochemical system; BMIM, 1-butyl-3-methylimidazolium hexafluorophosphate; CAs, carbon aerogels; CB, carbon black; CF, carbon-felt; CNTs, carbon nanotubes; COD, chemical oxygen demand; DFT, density functional theory; DMP, dimethyl phthalate; DMZ, dimetridazole; DSA, dimensional stable anode; EAOPs, electrochemical advance oxidation processes; EF, electro-Fenton; EIS, electrochemical impedance spectroscopy; Fe-CHI, Fe-chitosan; FCSW, iron contains sludge waste; FMBO, Fe-Mn binary oxide; GC, glassy carbon; GDE, gas diffusion electrode; GEF, goethite-catalyzed electro-Fenton process; Gr, graphite; Hetero-EF, heterogeneous electro-Fenton process; Hetero-PEF, heterogeneous photo electroFenton; FCA, Fe doped carbon aerogel; MCE, mineralization current efficiency; ADE, Ar diffusion electrode; *hv*, ultraviolet irradiation; LC-MS, liquid chromatography coupled with mass spectrometer; LDH, layered double hydroxide; MB, methylene blue; MFCs, microbial fuel cells; MTBE, methyl *tert*-butyl ether; NPs, nanoparticles; NTs, nanotubes; ·OH, hydroxyl radical; PEF, photo electro-Fenton; PEs, particle electrodes; p-NP, p-nitrophenol; POPs, persistence organic pollutants; PPY-AQDS, polypyrrole-anthraquinone-2,6-disulfonate; Pt, platinum; PTFE, polytetrafluoroethylene; QEEG, quinone-functionalized electrochemically exfoliated graphene; RB 19, Reactive Black 19; R<sub>ct</sub>, interfacial electron-transfer resistance; rGO, reduced graphene oxide; RhB, rhodamine B; ROS, reactive oxygen species; SAC, sludge derived activated carbon; SS, stainless steel; TOC, total organic carbon; UVC, short-wavelength ultraviolet; UVA, long-wavelength ultraviolet

\* Corresponding authors at: Laboratório de Electroquímica Ambiental e Aplicada, Instituto de Química, Universidade Federal do Rio Grande do Norte, Lagoa Nova, CEP 59.072-900, RN, Brazil.

E-mail addresses: [soliu.ganiyu@ccet.ufrn.br](mailto:soliu.ganiyu@ccet.ufrn.br) (S.O. Ganiyu), [carlosmh@quimica.ufrn.br](mailto:carlosmh@quimica.ufrn.br) (C.A. Martínez-Huitl).

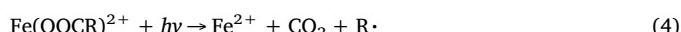
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members of this class of EAOPs are electro-Fenton (EF) and photo-electro-Fenton processes (PEF) [4,12–14]. The PEF is a photo-assisted upgrade of EF process which utilizes either ultra-violet (UVA and UVC), solar or visible light photoexcitation of  $\text{Fe}^{3+}$  complexes formed in Fenton's reaction (Eq. (1)) to produce both  $\text{Fe}^{2+}$  and  $\cdot\text{OH}$  (Eqs. (3) and (4)), thus it increases the quantities and regeneration of  $\cdot\text{OH}$  as well as the efficiency of the process [1,4,15,16]. The photogenerated  $\text{Fe}^{2+}$  ion can subsequently catalyzed the Fenton's reaction, forming  $\text{Fe}^{3+}$  and closing the cycle (Eq. (1)).



These processes are efficient for the complete degradation and excellent mineralization of synthetic and real wastewater contaminated with different class of organic pollutants such as pharmaceuticals and personal care products, endocrine disrupt compounds, pesticides, textile effluents, polycyclic aromatic hydrocarbons, surfactants and landfill leachates [1,5,7–9,12,14,16–18].

The major challenge of both EF and PEF is that both processes are only optimum at strong acidic pH conditions (*i.e.* pH 2.8–3.5), which are negative and disadvantageous from the environmental point of view, since a final neutralization step may become necessary to obtain tolerable effluents [19–22]. Besides, efficiency of EF and PEF significantly reduced when working outside pH 2.8–3.5. For instance at pH ≤ 2.5, the formation of peroxonium ions ( $\text{H}_3\text{O}_2^+$ ) which makes the electrogenerated  $\text{H}_2\text{O}_2$  electrophilic and reduces its reactivity towards  $\text{Fe}^{2+}$ , in addition to the preferential  $\text{H}_2$  evolution at the cathode occurs at lower acidic pH; whereas at pH ≥ 4.5, there is both gradual precipitation of  $\text{Fe}^{3+}$  (elimination of the catalyst) as ferric hydroxide and the decomposition of generated  $\text{H}_2\text{O}_2$  into water and  $\text{O}_2$ , thus hindering the production of  $\cdot\text{OH}$  [1,19]. Other challenge of homogeneous EF and PEF is the non-recyclability of the catalyst used, which made the technique unsuitable for continuous experimental process (Table 1).

Hetero-EF uses solid catalyst source for the decomposition of  $\text{H}_2\text{O}_2$  to form  $\cdot\text{OH}$ . It has been investigated as a promising alternative to homogeneous EF to overcome necessities for catalyst quantity optimization as well as widening the pH range at which EF process can be performed. This is beneficial because most real effluents encounter in nature are of wide and variable pH ranges and compositions, thus not suitable for EF and PEF treatments without adjusting the pH to strong acidic pH values [19]. Earlier effort to overcome the challenge of narrow pH window in EF resulted in the use of some naturally occur iron bearing minerals such as goethite and magnetite as heterogeneous catalysts for the treatment of synthetic wastewater [23,24]. Besides,

some of these iron minerals are pH regulator, meaning that they are capable of reducing the pH of the solution towards the strong acidic pH required for effective EF process [22,25]. In particular, pyrite and chalcopyrite has been successfully used to catalyze the degradation of some pharmaceuticals at circumneutral pH with higher removal and mineralization efficiency [25–28]. Many researches have also been tailored towards developing Fe-containing synthetic heterogeneous catalysts which are either used alone or supported on microporous or mesoporous materials for application in Hetero-EF treatment of organic pollutants in water [29–31]. Of recent, iron and/or transition metal oxides modified or functionalized cathodic materials have been prepared *via* various techniques for application in Hetero-EF process. In this case, the cathode performs dual function – as counter electrode as well as the iron source (catalyst) during the electrochemical treatment process. The functionalized cathode may be obtained by: (i) supported or immobilized iron source on a conductive materials (mostly carbonaceous material), (ii) chemically modified a conductive materials with iron source or (iii) one-pot or multistep chemically prepared low density porous solid materials containing iron and/or transition metals source (*i.e.* carbon aerogel) [19,20,32,33].

Generally, the degradation of organic pollutants during Hetero-EF involves two mechanisms – homogeneous catalyzed process by  $\text{Fe}^{3+}/\text{Fe}^{2+}$  redox couple dissolved into the solution and surface catalyzed process at the solid catalyst-liquid interface, depending on the working pH and nature of the catalyst used [19–21]. Up to date, comprehensive reviews on the Hetero-EF wastewater treatment are limited in literature. The only available chapter of a book on this topic recently published by Oturan group [22] mainly focuses on solid catalyst/supports solid catalyst without addressing the heterogeneous particle electrode and functionalized cathodic materials. Therefore, in this *exhaustive* review, the advantages of Hetero-EF and its main mechanism of production of  $\cdot\text{OH}$  were firstly presented, followed by the general features of good heterogeneous catalyst. The two main configurations of Hetero-EF that have been reported in literature were extensively discussed and a summary of relevant studies related to each configuration were presented. In the final section, current challenges and possible future strategies were discussed from the perspective of catalyst development/synthesis and process design. It is in our view that this review we increase the attention given to Hetero-EF for wastewater treatment and bring about further expansion of knowledge in this exciting area of electrochemical wastewater treatment.

## 2. Advantages of heterogeneous electro-Fenton process

Considering the challenges of homogeneous EF process for the remediation of organic pollutants, the most important advantage of Hetero-EF is its application over a wide pH range. In essence, several

**Table 1**

Comparison of advantages and drawbacks of Heterogeneous EF (Hetero-EF) and Heterogeneous PEF (Hetero-PEF) with other EAOPs.

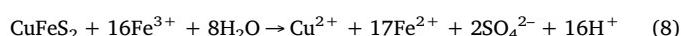
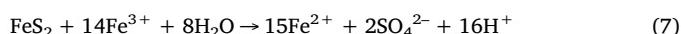
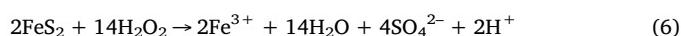
| Technology                        | Advantages   | Drawbacks   |
|-----------------------------------|--|---|
| Hetero-EF/Hetero-PEF              | Efficient over wide pH working window<br>Easy post treatment separation, reusability and recyclability of the catalysts<br>Possible regulation of solution pH towards strong acidic region<br>Easy automation<br>Suitable for the treatment of real wastewater | Possible additional cost due to solid catalyst production<br>Requires more careful materials/catalysts selection to avoid negative environmental impacts                                |
| Homogeneous EF/PEF                | Low quantity and cheaper catalyst source<br>Easy to operate compared to Hetero-EF/Hetero-PEF   | Efficient only at narrow pH window (pH 2.8–3.5)<br>Requires post-treatment neutralization of treated wastewater<br>Limited reusability and recyclability of the catalyst neutralization |
| Electrooxidation/Anodic oxidation | Requires no catalyst and less chemicals for operation<br><br>Efficient over wide pH window<br>Suitable for the treatment real wastewater provided non-active electrode is utilized   | Higher electrical energy consumption<br>Requires very expensive electrode material ( <i>i.e.</i> BDD)<br>Inferior efficiency compared to analogous EF/PEF and Hetero-EF/Hetero-PEF      |

**Table 2**  
some real wastewater/effluent with their pH.

| Type of real wastewater                    | pH range     |
|--|--------------|
| Building and construction chemical factory | 6.1–9.5 [34] |
| Plastic shoes manufacturing factory        | 5.6–7.8 [34] |
| Industrial dyeing effluent - Poland        | 11.2 [35]    |
| Textile wastewater – India                 | 10–12.2 [36] |
| Pharmaceutical wastewater                  | 3.9–9.2 [37] |
| Olive oil mill wastewaters                 | 4.5–6.5 [38] |
| Petrochemical wastewater                   | ≈5.6 [39]    |
| Landscape water                            | 7.2 [40]     |
| Brewery wastewaters                        | 7.5 [41]     |
| Alcoholic wastewater                       | 4.5–4.8 [42] |
| Wastewater from almond industry            | 6.2 [43]     |
| Reverse osmosis concentrate                | 8.3 [44]     |

Hetero-EF configuration and design have been reported to be practically pH independent. The circumventing of the pH limitation of classical EF process can ensure the easy application of Hetero-EF to wide range of real effluents without prior pH adjustment. Indeed, real wastewater or effluents are not only multi-components but also have wide pH variation depending on the industrial setup or origin. The pH of real effluents from some industrial plants and municipal wastewater are summarized in Table 2.

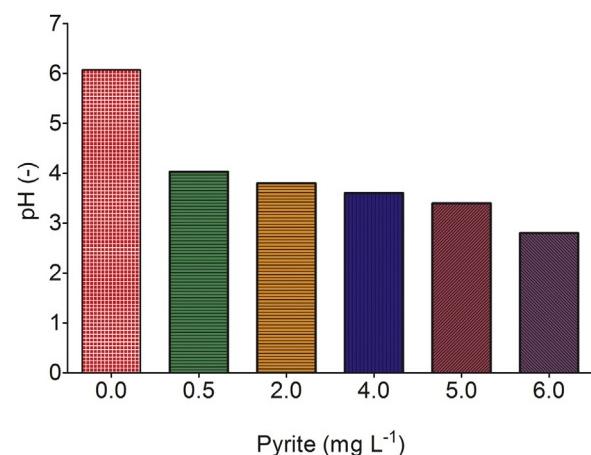
As seen in Table 2, majority of the effluents from industrial plants are either at strong basic or circumneutral pH, thus, homogeneous EF is not appropriate for the treatment of these wastewaters without prior pH adjustment. However, Hetero-EF is well suitable and efficient treatment technique for such pH-multi-variant effluents either as a single or mixture from different plants since the efficiency of most Hetero-EF design are pH independent. Based on previous studies [19–21], the independence of the efficiency of Hetero-EF has been achieved via two mechanisms: (i) using pH regulator as heterogeneous catalyst in the presence of O<sub>2</sub> and (ii) surface catalytical decomposition of H<sub>2</sub>O<sub>2</sub> to ·OH. In the case of pH regulator, the catalyst undergoes oxidation in the presence of O<sub>2</sub> with the accumulation of H<sup>+</sup> in the solution, thus decrease the solution pH towards the acidic values required for efficient EF process. The most common example of such catalyst is natural pyrite and chalcopyrite, which act as both iron ions source dosage and pH regulator and the mechanism is summarized in Eqs. (5)–(8) [25,28].



A typical pH regulating effect of natural pyrite is shown in Fig. 1 as reported by Labidha et al. [25].

On other hand, the catalytic decomposition of H<sub>2</sub>O<sub>2</sub> to ·OH at the surface of solid heterogeneous catalyst has been the main mechanism of degradation of organic pollutants at circumneutral and basic pH values because iron and/or transition metal used in catalytic Fenton's reaction are indissolvable at neutral or alkaline pH conditions [20]. This implies that with solid iron/transition metal source, the Hetero-EF can be efficiently carried out over a wide pH range. In particular, iron-supported catalyst and functionalized cathodic materials such as iron/transition metal containing carbon-aerogel exhibited such properties and demonstrated to achieve excellent mineralization efficiency during Hetero-EF treatment of different class of organic pollutants over wide pH range, including strong alkaline pH conditions of around 12 [45]. Detail of the surface catalyzed decomposition of H<sub>2</sub>O<sub>2</sub> to ·OH is given in the Section 3.

Related to the application over wide pH window is the elimination or inhibition of formation of iron hydroxides sludge during Hetero-EF process or post-treatment neutralization stage. This is important

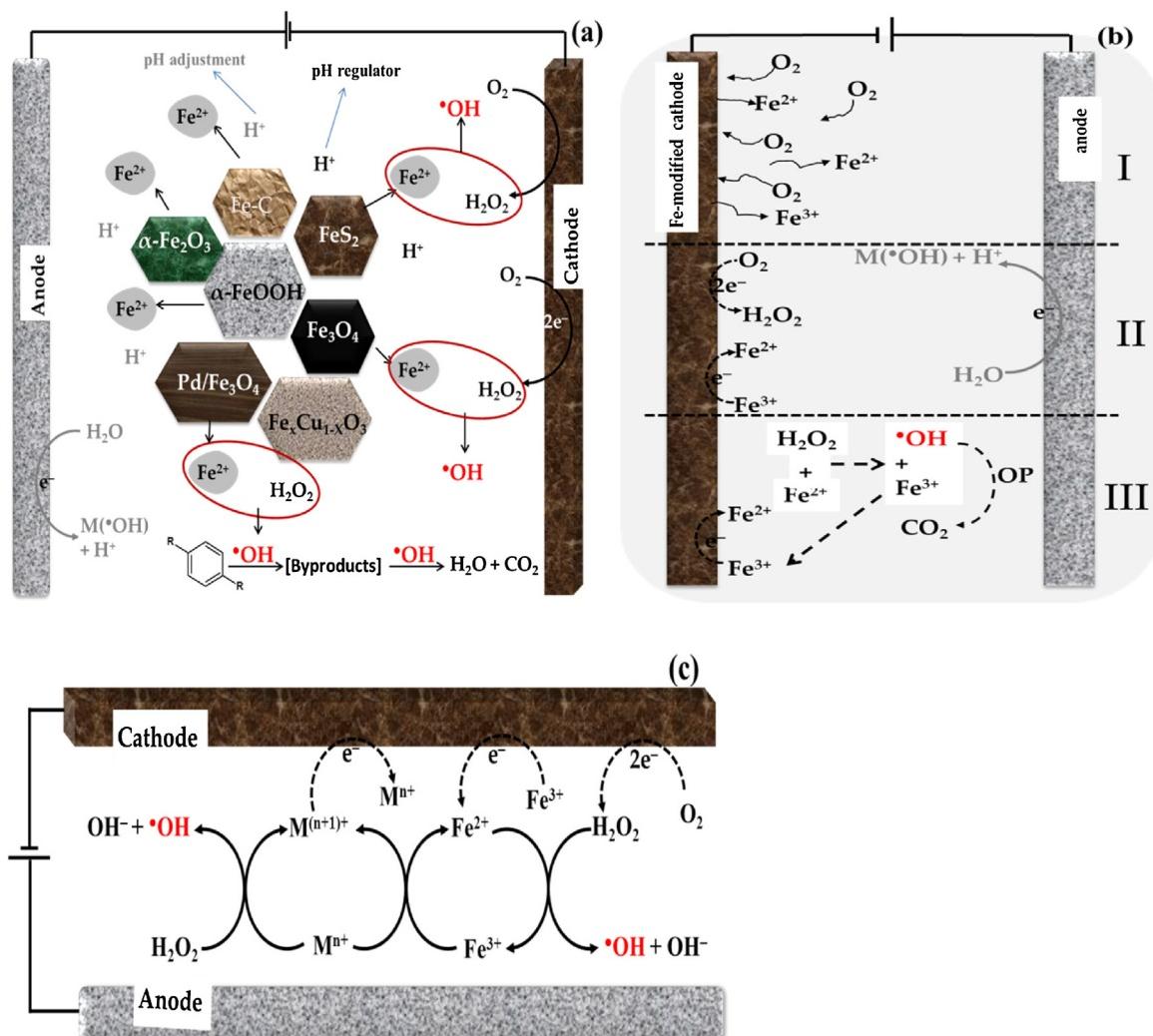


**Fig. 1.** Effect of pyrite suspension loading on the pH of 250 mL solution of 175 mg L<sup>-1</sup> APH synthetic dye in 0.05 M Na<sub>2</sub>SO<sub>4</sub> after 15 min.  
Printed with the permission of Ref. [25].

because the elimination of sludge could enhance the efficiency of the process (*i.e.* increases the availability of the catalyst) as well as reduced both energy consumption and overall cost of the process [21]. The formation of the sludge during conventional EF treatment implies the loss of the Fenton's catalyst, which has adverse effect on the process efficiency, whereas sludge formed during post-treatment neutralization of solution treated with EF may require further proper disposal. The use of Hetero-EF especially with iron supported or functionalized cathodic materials eliminate the formation of the sludge during the treatment regardless of the working pH conditions. Besides, Hetero-EF using solid catalyst or functionalized cathode allows easy separation and possible recycling of the iron promoter. This is an important parameter which ensures continuous operation of the treatment system unlike in homogeneous EF where the catalyst cannot be separated from the treated solution. Indeed, some studies have shown that functionalized cathodic materials like ferrite and Fe-Cu carbon aerogel and Fe-modified carbon-felt and graphite-felt can be repeatedly used in several cycles without significant reduction in the efficiency of the process, even up to ten (10) cycles [19,20,46]. The reusability and recyclability in Hetero-EF distinguished the process from homogeneous EF and enhance the efficiency of the system. It can also reduce the overall cost for the treatment of wastewater since the process can be easily adapted to automation.

### 3. Mechanism of heterogeneous electro-Fenton

According to literatures [47–49], the decomposition of H<sub>2</sub>O<sub>2</sub> by solid mono/mixed iron oxides, iron/transition metals containing compound and Fe-functionalized cathodic materials generally involves two situations according to the pH conditions at which electrolysis is being performed. At lower pH conditions (pH < 4.5), the process is controlled by the redox cycling of dissolved Fe<sup>3+</sup>/Fe<sup>2+</sup> and surface Fe<sup>III</sup>/Fe<sup>II</sup> couples (Fig. 2a and b). The dissolved Fe<sup>3+</sup>/Fe<sup>2+</sup> released from the leaching of significant quantities of iron ions for the solid catalyst or Fe – functionalized cathodic materials due to the acidic working pH conditions. Other transition metals redox couples such as Cu<sup>2+</sup>/Cu<sup>+</sup>, Co<sup>3+</sup>/Co<sup>2+</sup> and others could also catalyze the decomposition of H<sub>2</sub>O<sub>2</sub> to ·OH if leached from solid catalyst into treated solution (Fig. 2c) [19,50–53]. Besides, the presence of other transition metals in addition to iron in the solution may provoke reduction of Fe<sup>3+</sup> to Fe<sup>2+</sup> in conjunction with the catalytical decomposition of the H<sub>2</sub>O<sub>2</sub> as shown in Fig. 2c, thus enhance the efficiency of the electrolytic system [54–57]. At the same time under lower acidic pH conditions, H<sub>2</sub>O<sub>2</sub> decomposition could also be achieved by the surface alkalescent ≡Fe<sup>III</sup>/Fe<sup>II</sup> –OH at the surface of the solid catalyst [58,59]. Therefore, the predominant



**Fig. 2.** mechanism of catalytic activation of  $\text{H}_2\text{O}_2$  at acidic pH (pH ~ 3) using (a) supported or non-supported iron/iron-containing solid catalyst, (b) iron-functionalized cathodic materials (I: adsorption of dissolved  $\text{O}_2$  and leaching of iron ions; II: electrogeneration of  $\text{H}_2\text{O}_2$  and regeneration of  $\text{Fe}^{2+}$  from reduction of  $\text{O}_2$  and  $\text{Fe}^{3+}$  respectively and III: Fenton's production of  $\cdot\text{OH}$ ) and (c) proposed participation of other transition metals in redox recycling of iron ions and catalytic decomposition of  $\text{H}_2\text{O}_2$  ( $\text{M} = \text{Cu}, \text{Mn}, \text{Co}, \text{V}, \text{Ti}, \text{Ni}$  or  $\text{Nb}$ ).

Adopted from Refs. [60,21,57,83] respectively.

catalytic process not only depends on the working pH but also on the solubility of the solid catalyst at lower pH [31]. Solid catalysts such as natural iron minerals [23,27,60–62] as well as synthetic nanoparticles of iron and iron supported catalysts [21,29,58,63–74] undergoes excessive leaching of iron ions at acidic pH especially pH  $\leq 3$  at which Fenton's reaction is optimum, thus  $\text{H}_2\text{O}_2$  decomposition is majorly by homogeneous  $\text{Fe}^{3+}/\text{Fe}^{2+}$  catalyzed mechanism. Depending on the cathode materials used, the homogeneous redox couples may be continuously regenerated at cathode (Eq. (9)), thus making the system a close loop [75–79].



Similar behavior has been reported for some iron/transition metal containing functionalized electrode such as Fe- bentonite particle electrode,  $\text{Fe}@\text{Fe}_2\text{O}_3/\text{ACF}$ , Fe-Carbon-felt, Fe and Fe-Cu allophane nanoclays with large quantities of leached iron ions, which can catalyze the  $\text{H}_2\text{O}_2$  decomposition in the bulk with minimum surface decomposition of  $\text{H}_2\text{O}_2$  [21,33,80–82]. It is important to note that there is possibility of oxidation of  $\text{Fe}^{2+}$  and other transition metals ions at the anode surface during the electrolysis, however, this reaction is very insignificant and rarely reported in literature.

Other functionalized cathodic materials especially iron/transition

metal containing carbon-aerogel and layered double hydroxide modified carbon-felt exhibited relatively good stability at acidic pH and the leached iron ions concentration are usually relatively minimal [19,45,84]. As such, surface catalyzed decomposition of  $\text{H}_2\text{O}_2$  by  $\text{Fe}^{\text{III}}/\text{Fe}^{\text{II}}$  is relatively significant when those functionalized cathodic materials are utilized in Hetero-EF at low acidic pH conditions. In summary, under these circumstances, the catalytic decomposition of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  is by homogeneous  $\text{Fe}^{3+}/\text{Fe}^{2+}$  and surface  $\text{Fe}^{\text{III}}/\text{Fe}^{\text{II}}$  redox couple, but the predominant process is determined by the nature of the solid catalyst used (i.e. solubility with pH).

In contrast, at neutral and alkaline pH values, the contribution of dissolved iron ions to the  $\text{H}_2\text{O}_2$  activation is expected to be negligible since  $\text{Fe}^{\text{III}}$  is insoluble [85,86]. Although the kinetics of Hetero-EF is complex and involved several parameters, but the most critical step is surely the production rate of  $\cdot\text{OH}$  from  $\text{H}_2\text{O}_2$ , which in this case is controlled by the solid catalyst properties,  $\text{H}_2\text{O}_2$  generation and solution pH [87–91]. Till date, no consensus reaction mechanisms is available in literature for the entire oxidation process, however, it is widely accepted that the Hetero-EF catalysis can fit the Haber-Weiss circle mechanism, which is similar to those observed in the classical homogeneous Fenton's reaction [20,92,93]. The surface-based mechanism is summarized by reactions in Eq. (10)–(20).

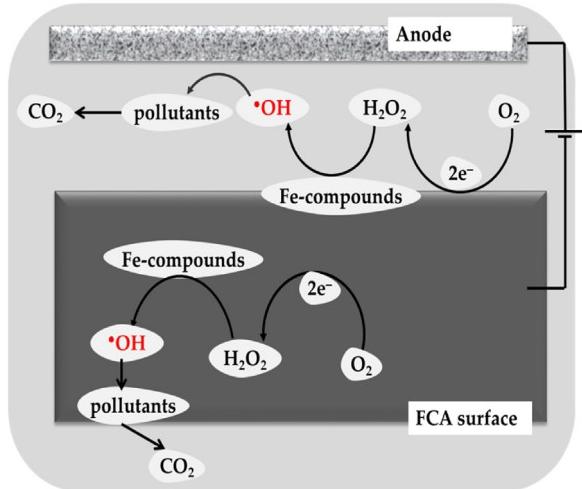
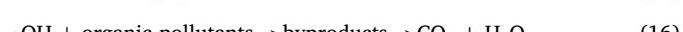
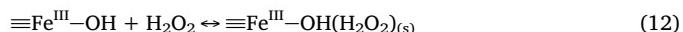


Fig. 3. mechanism of surface catalyzed activation of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  at neutral and basic pH on Fe-functionalized cathodic materials (here ferrite-carbon aerogel).

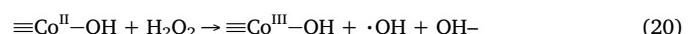
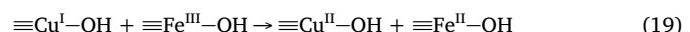
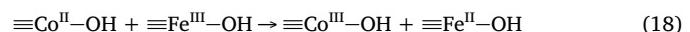
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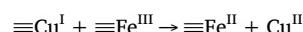
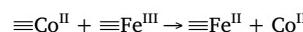
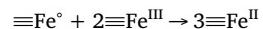
The surface-catalyzed mechanism (Fig. 3) is initiated with the generation of  $\text{H}_2\text{O}_2$  at/within the cathode and simultaneous partial reduction of  $\equiv\text{Fe}^{\text{III}}-\text{OH}$  at the surface of the Fe-containing catalyst to  $\equiv\text{Fe}^{\text{II}}-\text{OH}$  by obtaining one electron (Eqs. (10) and (11)) as current is applied across the system [20,45,94]. The generated  $\text{H}_2\text{O}_2$  can interact strongly with the negatively charged catalyst surface, forming a precursor surface complex  $\equiv\text{Fe}^{\text{III}}-\text{OH}(\text{H}_2\text{O}_2)$  within the inner and outer surface of the cathode matrix [95]. More so, the surface  $\text{H}_2\text{O}_2$  complex may be transformed into  $\equiv\text{Fe}^{\text{II}}-\text{OH}(\text{HO}_2\cdot)$  via reversible ground state electron transfer from the ligand to central atom (Eq. (13)), followed by deactivation to form  $\equiv\text{Fe}^{\text{II}}-\text{OH}$  (Eq. (14)) [20,61,62,92,93]. It is obvious that the rate of reactions in Eqs. (13) and (14) can be significantly accelerated by increasing the pH towards alkaline conditions, since the rapid consumption of  $\text{H}^+$  will swiftly shift the equilibrium towards the formation of more  $\equiv\text{Fe}^{\text{II}}-\text{OH}$  [30]. After that,  $\text{H}_2\text{O}_2$  is directly and catalytically decomposed by  $\text{Fe}^{\text{II}}$  to  $\cdot\text{OH}$ , which can oxidize the organic pollutants until their complete mineralization to  $\text{CO}_2$  and  $\text{H}_2\text{O}$ . The  $\cdot\text{OH}$  can also react with excess  $\text{H}_2\text{O}_2$  (quenching) to produce hydroperoxyl radical ( $\text{HO}_2\cdot$ ) (Eq. (17)), which is a much weaker oxidant compared to  $\cdot\text{OH}$ , thus reducing the efficiency of the process.

Other transition metal especially Co and Cu may also catalyze the decomposition of  $\text{H}_2\text{O}_2$  via surface mechanism as reported for  $\text{Co}^{\text{II}}\text{Fe}^{\text{III}}\text{LDH}$  modified carbon-felt [19],  $\text{Fe}_{3-x}\text{Cu}_x\text{O}_4$  nanoparticles [96], Fe-Co and Fe-Cu carbon-aerogel [84,97]. In this case,  $\equiv\text{Fe}^{\text{II}}-\text{OH}$  reduzate could be formed by an electron reduction of  $\equiv\text{Fe}^{\text{III}}-\text{OH}$  by both  $\text{Co}^{\text{II}}-\text{OH}$  and  $\text{Cu}^{\text{I}}-\text{OH}$  according to Eqs. (18) and (19). Additionally, direct decomposition of  $\text{H}_2\text{O}_2$  through  $\text{Co}^{\text{II}}-\text{OH}$  and  $\text{Cu}^{\text{I}}-\text{OH}$  catalysis to generate  $\cdot\text{OH}$  could be also achieved at the surface of the transition metals-containing solid catalyst (Eqs. (20) and (21)). Overall, transition

metal-co-catalyst provided two added advantage in Hetero-EF: (i) accelerate the production of the  $\equiv\text{Fe}^{\text{II}}-\text{OH}$  for  $\text{H}_2\text{O}_2$  decomposition (Eqs. (18) and (19)) and (ii) increased the rate of catalytic decomposition of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  like in the case of homogeneous EF [19,98–100].



Studies have shown that the production rate of  $\cdot\text{OH}$  in homogeneous Fenton reaction catalyzed by  $\text{Fe}^{2+}$  is 104–105 folds faster than  $\text{Fe}^{3+}$  catalyzed Fenton-like process [20]. On the other hand, the surface catalytic centers of Fe in iron oxide nanoparticles were reported to be at least 50-folds more effective for  $\cdot\text{OH}$  generation than dissolved  $\text{Fe}^{3+}$  ions at circumneutral pH [83,101]. This implies that the reduction of  $\text{Fe}^{\text{III}}$  to  $\text{Fe}^{\text{II}}$  at the surface of the catalyst is the rate-limiting step of the whole Hetero-EF reactions [20]. Previously, Costa et al. [102] and Moura et al. [88] have drawn similar conclusions when zero valent iron ( $\text{Fe}^{\circ}$ ) and iron oxides encapsulated composite were studied, which had higher reactivity in oxidation of organic pollutants than  $\text{Fe}^{\circ}$  or iron oxides alone due to the  $\text{Fe}_{\text{surf}}^{2+}$  species formation via electron transfer from  $\text{Fe}^{\circ}$  to  $\text{Fe}^{3+}$  within the composite and increased oxygen vacancies [103]. In 2013, Wang and co-workers [20] have also shown that the formation of  $\text{Fe}^{\text{II}}$  mediator with high catalytic activity for  $\text{H}_2\text{O}_2$  decomposition to  $\cdot\text{OH}$  was via reversible redox by electron transfer among the iron species with different valences (Eq. (22)) in a ferrite-carbon aerogel containing mix phase of  $\text{Fe}^{\circ}$  and  $\alpha\text{-Fe}_2\text{O}_3$ . The higher catalytic activity of Hetero-EF process arises from the formation of more  $\equiv\text{Fe}^{\text{II}}$  mediator via electron transfer among the iron species as shown in  $\text{Fe}^{\circ}$  and iron oxides composite and ferrite-carbon aerogel. This can also explain the higher catalytic activity and role of Co and Cu co-catalyst in  $\text{Fe}/\text{Cu}$  and  $\text{Fe}/\text{Co}$  functionalized cathodic materials since the addition of Co or Cu led to the formation of more  $\equiv\text{Fe}^{\text{II}}$  mediator as depicted in Eqs. (23) and (24).



#### 4. Required features of efficient heterogeneous catalyst

Wide varieties of substrates/materials can be selected as model catalyst and range of reaction conditions may be involved, therefore it is necessary to enumerate what would be the most important parameters that should be determined in order to rate different materials based on their activity to catalyze the decomposition of  $\text{H}_2\text{O}_2$  in Fenton's or Fenton's-like reaction [104]. The most important parameter is the catalytic activity and stability of the material over wide experimental conditions. The material should possess good catalytic activity which must be less affected by experimental conditions, especially pH, and high stability to ensure the reusability in several runs [83,91,104–106]. It is important to note that reusability in several runs is not a good criterion to assess stability of the catalyst because pollutant-to-catalyst ratio usually determines the reusability of the catalyst [107]. This implies that for solid catalyst with high stability, large excesses quantities would allow possible reusability of the catalyst in several consecutive reactions runs, whereas less amount of solid catalyst may make reusability more difficult. Optimization of the quantities of the catalyst may be necessary because excess material could enhance the destruction of the generated  $\cdot\text{OH}$  by its destructive attack on the catalyst especially when utilizing materials with low stability [104,108]. The optimum quantity of solid catalyst required for certain

wastewater treatment is closely related to the catalytic activity/properties of the solid, treated volume as well as organic matter content of the wastewater. The measurement of the maximum productivity of the catalyst may also be necessary considering the varieties and amount of solid catalyst used in Hetero-EF. Navalon et al. [104] has proposed a simple test in which a large excess substrate is used in a prolonged experiment until total deactivation of the catalyst. The data obtained will not only provide the maximum productivity but also information about the causes of deactivation of the catalyst. It may also necessary to wash the catalyst under alkaline conditions because the metal ions may form complexes with carboxylic acids, which are usually the final end organic products of electrochemical oxidation of organic pollutants. Besides in Hetero-PEF, the support material on which the catalysts (catalyst supported or impregnated on substrates) are deposited must be photo-resistant and non-radical scavenger to avoid degradation of the support.

Closely related to the stability of the catalysts as well as reusability is the absence of leaching of metal species from solid catalyst or deactivation/mechanical wearing of catalyst from the solid support into the aqueous phase, which is one key issue because it determines the contribution of homogeneous EF to the catalysis of the  $\text{H}_2\text{O}_2$  [104,109,110]. Minimum concentration of metal species could be afforded in the solution because the species can act as homogeneous catalyst. In the case, where there is significant leaching or mechanical wearing of the solid catalyst, the overall catalytic activity could be the combination of the activity of the leached species and solid catalyst. This was the case observed at pH 2 for  $\text{Co}^{II}\text{Fe}^{III}$ LDH functionalized carbon-felt [19,111], electrochemically prepared iron-modified activated carbon electrode [112] and other solid catalysts [113,114]. On the other hand, excessive leaching of metal species from solid catalyst may enhance the efficiency of Hetero-EF process especially at acidic pH conditions, at which Fenton's reaction is optimum, thus the system proceeds like a typical homogeneous EF process. The major disadvantage of leaching is depletion of the active metal sites in the solid catalysts which decreases the reusability, and if persisted for long time, it will cause the loss of the solid catalytic activity [104,115].

In the case of functionalized cathodic materials, the electrochemical properties of the modified material are an important parameter which can influence the performance of the Hetero-EF system. The nature and quantity of the solid catalyst grafted on the cathode material as well as the preparation route should have minimum negative effect on its conductivity since this could affect the charge transfer at liquid-solid interface and may reduce the potential of the material for production of  $\text{H}_2\text{O}_2$ . Most iron/transition metals compounds have lower conductivity than minimum required for EF cathode materials, as such reduces the electrical conductivity (increased electron-transfer resistance) of carbonaceous materials commonly used in EF when grafted or functionalized with these oxides. In most cases, the reduction in the conductivity is very significant but still within the limit required for successful electrochemical process, even though the effect of cathode modification on electron-transfer resistance depends on the compound grafted on the cathode. For instance, interfacial electron-transfer resistance ( $R_{ct}$ ) for raw carbon-felt determined by electrochemical impedance spectroscopy (EIS) was  $2.3 \Omega$  but it reduced to  $0.97 \Omega$  after modification with  $\text{Co}^{II}\text{Fe}^{III}$ LDH (Fig. 4), indicating a substantial reduction in electron-transfer resistance of the cathode and consequently, improving the electrochemical properties of the cathode [19]. Contrast results were observed for carbon-aerogel with the  $R_{ct}$  values of  $3.8 \Omega$  and  $75.8 \Omega$  obtained for pure and ferrite-doped carbon-aerogel respectively, demonstrating a reduction in electrochemical properties of prepared cathode [20].

Additionally, the substrate used to support the solid catalyst or the cathode material modified by iron compound should be non-reactive (physically or chemically) with  $\text{H}_2\text{O}_2$  since the efficiency of the Hetero-EF system is not only determined by the activity of the catalyst but also on the concentration/production rate of  $\text{H}_2\text{O}_2$ . Therefore, prior

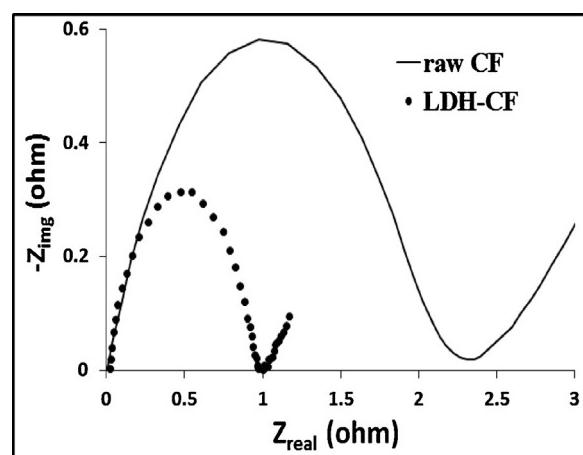


Fig. 4. EIS spectral of raw and  $\text{CoFe}^{II,III}$ LDH modified carbon-felt performed in 50 mM  $\text{Na}_2\text{SO}_4$  solution at voltage amplitude of 10 mV in the frequency range of 50 kHz to 100 MHz.

Adopted and printed with the permission of Ref. [19].

experiments are required to evaluate either the decomposition of the  $\text{H}_2\text{O}_2$  by the substrate used as support for the catalyst and products formed or the capacity of functionalized cathodic material for production of  $\text{H}_2\text{O}_2$ .

Further, the toxicity and environmental compatibility of the solid catalyst are other important parameters that should be considered for materials selected as catalysts or as supports for the catalyst. Iron oxides and supported Fe-compounds are considered more environmental friendly and exerted no toxicity in environment; as such leaching of iron ions into the solution and its subsequent disposal and the residual solid catalyst into surface water and/or environment has limited environmental consequences to ecosystem. However, recently other transition metals like copper, manganese, vanadium, nickel and cobalt have been used along with iron/iron oxides as solid catalyst in Hetero-EF [96,116]. In this case, the disposal of the treated solution or the residual solid catalysts may have serious environmental implications since these metals ions are considered toxic especially cobalt. Therefore, careful selection of catalyst/support materials is needed to avoid use of materials with questionable environmental compatibility as solid catalyst/support in Hetero-EF system. Additionally, exclusive description of the preparation procedure and explicit characterization data are other parameters that should be considered in order to ensure reproducibility of the material and the catalytic performance [104]. The catalyst-supported catalyst or functionalized cathodic materials for Hetero-EF should have easy production or fabrication route as well as a cost effective for possible adaption on commercial scale. Studies on catalyst-supported catalyst or functionalized cathode materials with complex and expensive route may only end-up on laboratory or pilot scale, because treatment of organic pollutants in wastewater or recycling water system is considered as a non-profit but essential stage of production, which may only become necessary in order to comply with environment regulation of the country. As such techniques or processes with minimum cost implication are usually preferred even if it is less effective.

Finally, based on the above explanation, it is clear that to propose a material as potential heterogeneous catalyst-supported catalyst or functionalized cathodic materials, extensive studies are required to determine the experimental conditions range in which the materials can exhibit catalytic activity and stability, extent of leaching at these conditions, interaction of support with the  $\text{H}_2\text{O}_2$  and the environmental compatibility of the solid catalyst and/or support. For functionalized cathodic materials, it is advisable to present the electrochemical properties along with description of synthesis procedures and well-founded characterization data.

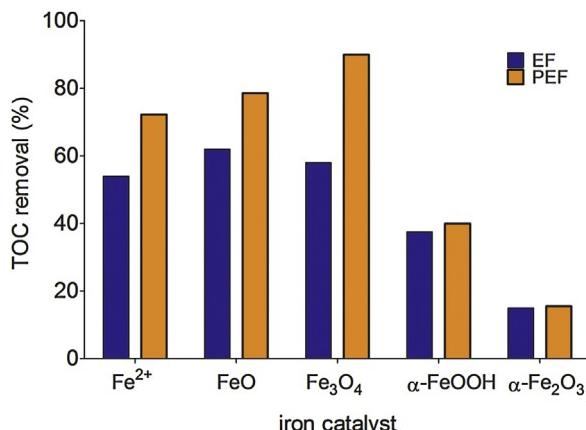
## 5. Hetero-EF with catalytic addition

Hetero-EF process with catalytic addition utilized solid catalysts which are natural or synthetic, relatively insoluble iron or iron-containing compound with or without supported on substrate to catalyze the decomposition of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$ . As stated earlier, the overall aim is to achieve reusability of the catalyst, easy separation after EF treatment and widening the pH window at which EF can be performed. The catalytic activity is usually the combination of homogeneous metal-ions and heterogeneous surface catalyzed process because extensive leaching of metal ions into the solution occurs especially when perform Hetero-EF at around pH 3 [22,117]. The solid catalysts that have been investigated in literature are grouped into two – natural minerals and synthetic iron-containing nanoparticles/iron-supported solid catalysts. The details of the studies are provided in Sections 5.1 and 5.2.

### 5.1. Natural minerals

Several studies have demonstrated the potential of some solid iron-bearing natural minerals to catalyze the decomposition of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  and in turn, mineralization of different class of organic pollutants. In most cases, the systems allow expanding the working pH window to neutral media and preventing the accumulation of iron sludge. Pioneer studies investigated the viability of goethite ( $\alpha\text{-FeOOH}$ ) as a solid heterogeneous iron catalyst source for the mineralization of aqueous aniline solution in a modified EF process termed “goethite-catalyzed EF (GEF) process [23]. At optimum EF conditions, 95% mineralization was attained with the GEF process, suggesting  $\alpha\text{-FeOOH}$  as a suitable solid iron dosage source for Hetero-EF process. Subsequent work [24] by the same group reported the catalytic behavior of other iron oxides minerals such as wustite ( $\text{FeO}$ ), magnetite ( $\text{Fe}_3\text{O}_4$ ) and hematite ( $\alpha\text{-Fe}_2\text{O}_3$ ) for the catalytic decomposition of  $\text{H}_2\text{O}_2$  in both EF and PEF processes. Graphical representation of TOC removed after 5 h of EF treatment of 100 mg L<sup>-1</sup> aniline solutions with 1 g L<sup>-1</sup> of these solid catalysts or 0.5 mM Fe<sup>2+</sup> using Pt/GDE cell is shown in Fig. 5. It was observed that only wustite (62%) and magnetite (58%) achieved more TOC removal than Fe<sup>2+</sup> (54%) during the EF treatment, whereas the catalytic efficiency of goethite and hematite was much lower. The trend in the TOC removal efficiency was related to the ability of the solid iron oxides to release Fe<sup>2+</sup> to the bulk to catalyze the activation of electrogenerated  $\text{H}_2\text{O}_2$  through Fenton's reaction (Eq. (1)), so the system behave as pure homogeneous EF process with the solid catalyst acts as self-regulator of iron dosage.

In a recent collaboration works between Oturan, Brillas and Ammar



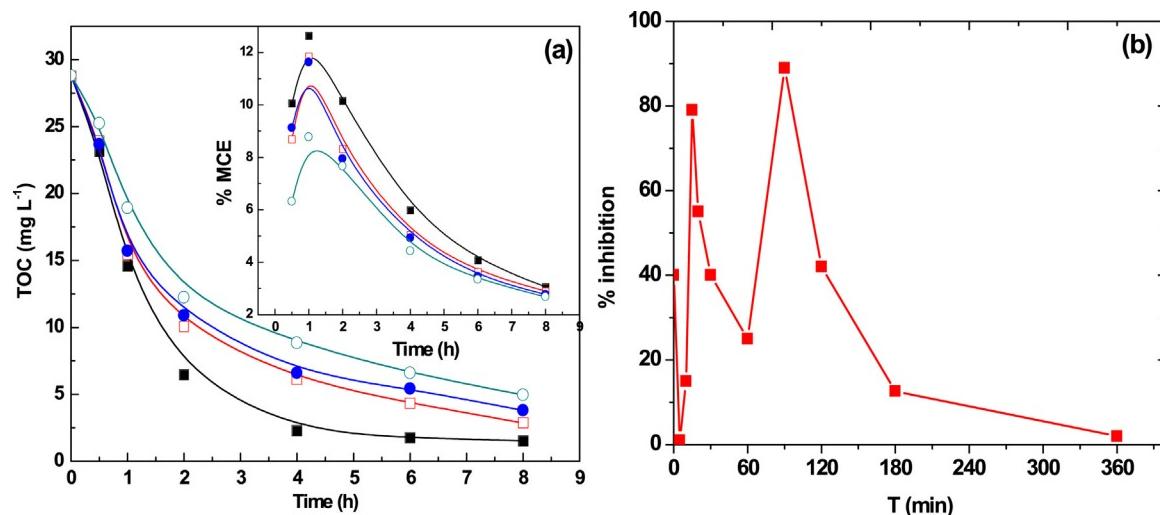
**Fig. 5.** comparison of TOC removal achieved after 5 h of EF and PEF treatment of 100 mg L<sup>-1</sup> aniline solutions containing 0.2 M Na<sub>2</sub>SO<sub>4</sub> at pH 3, 0.5 L min<sup>-1</sup> air flow, and 250 mA applied current in Pt/GDE cell using 0.5 mM of Fe<sup>2+</sup> or 1 g L<sup>-1</sup> of solid iron catalyst.

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groups, natural pyrite and chalcopyrite have been studied as a sustainable solid heterogeneous catalyst and pH regulator for the mineralization of different classes of organic pollutants [26]. For instance, Labiad and co-workers [25] studied natural pyrite as heterogeneous solid iron dosage for the mineralization of new synthetic dye 4-Amino-3-hydroxy-2-p-tolylazonaphthalene- 1-sulfonic acid (AHPS) in an undivided reactor equipped with boron doped diamond (BDD) anode and carbon-felt cathode. The authors observed that the dissolution of the pyrite sharply reduced the pH of the solution from 6.07 to between 4.03–3.0 within the first 10 min after adding 0.5–6.0 mg L<sup>-1</sup> pyrite; and it further decreases to 3.9–2.8 after 15 min at similar dosage using 230 mL of solution. Over 90% mineralization efficiency was attained after 5 h of electrolysis with 2.0 g L<sup>-1</sup> of pyrite dosage at applied current of 300 mA, whereas analogous studies with homogeneous EF using 0.45 mM Fe<sup>2+</sup> could only attained 70% mineralization at the same electrolysis time. Further studies by the same group [28] have shown that the addition of 1.0 g L<sup>-1</sup> pyrite dosage to aqueous solution of tyrosol adjusts easily the solution pH to around 3 and provided approximately 0.2 mM Fe<sup>2+</sup> to catalyze the so called EF-pyrite system. Comparative studies using 0.2 mM Fe<sup>2+</sup> and 1.0 g L<sup>-1</sup> pyrite dosage for conventional EF and EF-pyrite, respectively, at 50 mA, showed that the mineralization efficiency attained by EF-pyrite was approximately 5.8 times higher than that obtained in conventional EF. The superior efficiency of EF-pyrite was attributed to the “self-regulation” of the Fe<sup>2+</sup> ions in the system by the pyrite as explained in Section 2. In related studies, the EF-pyrite process was also investigated for the mineralization of antibiotics levofloxacin [27], sulfamethazine [26], tetracycline [61,118] and phenolic compound, vanillic acid [119] with the TOC removal efficiency always higher for EF-pyrite compared to conventional EF, at similar experimental conditions for the pollutants studied. In particular, the mineralization efficiency obtained in EF-pyrite with Pt was quiet similar to those attained in convention EF with BDD anode during the treatment of sulfamethazine, which is very exciting consider the cost of BDD anode (Fig. 6a). The group [60] also shown that complete detoxification of sulfamethazine and tetracycline could be achieved at optimum experimental conditions and the pyrite itself have exhibited no toxicity/inhibition to bacteria *V. fischeri* used in microtox® analyses (Fig. 6b).

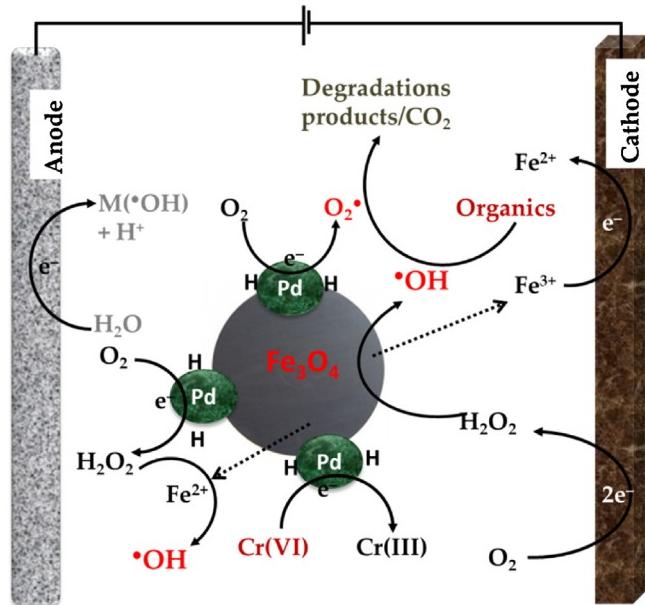
### 5.2. Synthetic iron/iron-containing nanoparticles/supported solid catalysts

Synthetic iron oxides and iron-contained nanoparticles and supported solid catalysts have been investigated for the Hetero-EF treatment of different classes of organic pollutants. The mechanism of decomposition of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  is similar to that of natural iron mineral catalyst, which is a combination of homogeneous catalyzed process by leached/dissolved Fe<sup>2+</sup>/Fe<sup>3+</sup> redox cycle from the solid catalyst and surface catalysis at the solid-liquid interface with some few exceptions. The synthesis techniques varies from one solid catalyst to other and extensive characterization of these catalysts are most studied along with their catalytic activity [91,120]. For instance, Hou et al. [29] investigated synthetic nano- $\text{Fe}_3\text{O}_4$  for the Hetero-EF oxidation of catechol with the aim of evaluating the effect of operating parameters such as temperature, pH, current density, catalyst loading, initial catechol concentration as well as reusability of the nano- $\text{Fe}_3\text{O}_4$ . The degradation efficiency of catechol was found to decreases with pH, but satisfactory efficiency was still attained at pH 6. Initial catechol concentration did not affect its removal efficiency, but the efficiency increases with the  $\text{Fe}_3\text{O}_4$  loading within the range studied (0.25–2.0 g L<sup>-1</sup>). Besides, less than 10% of reduction in degradation and mineralization efficiency was observed after 8 cycles of reuse, demonstrating the high stability and reusability of the nano- $\text{Fe}_3\text{O}_4$  in Hetero-EF process. Other research groups [121–125] have also utilized  $\text{Fe}_3\text{O}_4$  nanosphere supported Pd (i.e. Pd/ $\text{Fe}_3\text{O}_4$ ) as solid heterogeneous catalyst for the simultaneous generation of  $\text{H}_2\text{O}_2$  and catalytic decomposition of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  (Fig. 7). The synthesized Pd/ $\text{Fe}_3\text{O}_4$  showed efficient mineralization of



**Fig. 6.** (a) TOC decay vs electrolysis time for the mineralization of 200 mL of 0.2 mM sulfamethazine solution in 0.05 M  $\text{Na}_2\text{SO}_4$  at pH 3, 300 mA and room temperature using undivided (●, ○) Pt/CF and (■, □) BDD/CF cells with (●, ■) 1 g  $\text{L}^{-1}$  pyrite and (○, □) 0.2 mM  $\text{Fe}^{2+}$ . The corresponding MCE is shown in the inset panel. (b) Evolution of solution toxicity assessed in terms of percentage inhibition of the luminescence of *V. fischeri* bacteria after 15 min of exposure during electrolysis at the same conditions as (a) using BDD/CF cell.

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**Fig. 7.** Proposed mechanism of humic acids and Cr (VI) removal using  $\text{Pd}/\text{Fe}_3\text{O}_4$  catalyst.

Adapted from Ref. [122].

pentachlorophenol [124] as well as simultaneous removal of Cr (VI) and degradation of humic acids in aqueous solution [122]. Complete removal of pentachlorophenol was attained in 30 min at applied voltage of 5 V, pH 2.8 and 288 k with  $\text{Pd}/\text{Fe}_3\text{O}_4$  compared to 17.2% obtained with electrochemical oxidation treatment alone; and approximately 90% of mineralization of humic acids and higher Cr (VI) removal efficiency was attained at the optimal experimental conditions. The  $\text{Pd}/\text{Fe}_3\text{O}_4$  nanocatalyst acts as electron and hydrogen atoms transfer carrier and the oxidation of organics was performed by the participation of  $\text{O}_2$  and  $\cdot\text{OH}$ , whereas the reduction of Cr (VI) was attribute to the contribution of  $\text{Pd}/\text{Fe}_3\text{O}_4$  nanocatalyst and the atomic hydrogen on the catalyst surface (Fig. 7). The Pd nanoparticles anchor on the  $\text{Fe}_3\text{O}_4$  nanosphere was found to enhanced the atomic hydrogen and  $\text{H}_2\text{O}_2$  production and in turns Cr (VI) and humic acids removal efficiency up to 5 wt%, whereas no essential change in efficiency was found at higher

Pd loading. Meanwhile, the catalytic activity of the  $\text{Pd}/\text{Fe}_3\text{O}_4$  deteriorated severely with use due to difficulty in recovery of the nanoparticles, thus limited the reusability of the catalyst. The catalyst has also been studied for the degradation of phenol [123], 4-bromophenol [121], Rhodamine B [126] and trichloroethylene in groundwater [127]. Other studies have utilized nanostructured Pd/Fe modified graphene [128] and Pd/Fe nanoscale particles [129] for degrading chlorinated phenols. In most cases, the Pd nanoparticles catalyzed the combination of  $\text{H}_2$  and  $\text{O}_2$  electrogenerated at the cathode and anode respectively to  $\text{H}_2\text{O}_2$  according to Eqs. (25)–(28) [122–124,130], which is an important reagent for Fenton's reaction.



Some authors have also studied  $\text{Fe}_2\text{O}_3$ /supported- $\text{Fe}_2\text{O}_3$  nanoparticles or solid catalysts for Hetero-EF degradation of organic pollutants. For example, Yue et al. [131] investigated  $\alpha\text{-Fe}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  nanocatalyst for degrading 500 mg  $\text{L}^{-1}$  of Acid Red 3R and the decolorization efficiency of 77.2% was attained in 100 min at optimum conditions of pH 3, 0.2  $\text{m}^3 \text{h}^{-1}$  airflow and 20 V applied constant voltage. The LC-MS analysis of the treated solution showed that the azo dye was firstly degraded into aromatic intermediates, followed by ring opening into carboxylic acids before final mineralization to  $\text{CO}_2$ . Recently, Ozcan and co-workers [132] reported the efficiency of  $\text{Fe}_2\text{O}_3$  modified kaolin for Hetero-EF degradation of antibiotic enoxacin. The mineralization rate of enoxacin attained its maximum value at 0.3 g  $\text{Fe}_2\text{O}_3$ -kaolin loading, pH 2.0–3.0 and applied current of 300 mA. Interestingly, complete mineralization of enoxacin were also obtained at pH 5.1 and 7.1 and less than 0.5% reduction in mineralization efficiency was observed after 5 cycles of reuse, demonstrating the efficiency of the catalyst over wide pH range and its high recyclability.

Two Chinese research groups have also studied iron containing perovskite-like solid catalysts  $\text{ZnFe}_2\text{O}_4$  [133] and  $\text{Bi}_2\text{Fe}_4\text{O}_9$  [134] for the Hetero-PEF and Hetero-EF degradation of benzotriazole and 1-diazo-2-naphthol-4-sulfonic acid, respectively. Heterogeneous PEF using  $\text{ZnFe}_2\text{O}_4$  showed high catalytic activity for degrading benzotriazole

with 91.2% and 85.3% for degradation efficiency and COD removal, respectively, after 180 min of treatment at optimum experimental conditions with graphite electrodes. The benzotriazole degradation efficiency and COD removal decreased with an increase in pH and initial benzotriazole concentration; but increased with  $ZnFe_2O_4$  dosage in the range of 0–0.067 g L<sup>-1</sup> and applied negative voltage between -0.3 to -0.6 V. Similar results were observed during the Hetero-EF process in a reactor equipped with Ti/GDE electrodes using  $Bi_2Fe_4O_9$  as catalyst, however, the degradation efficiency of 1-diazo-2-naphthol-4-sulfonic acid and COD depletion depended on the solution pH,  $Bi_2Fe_4O_9$  dosage and applied current. At optimum conditions, almost complete COD removal (89%) was achieved after 200 min of treatment, whereas comparative electrochemical oxidation (without  $Bi_2Fe_4O_9$ ) and adsorption (with  $Bi_2Fe_4O_9$ ) studies merely attained 39% and 32% COD removal, respectively, at similar treatment time. Other group [95] has also investigated the catalytic activity of  $Fe_{3-x}Cu_xO_4$  ( $0 \leq x \leq 0.25$ ) nanoparticles prepared by co-precipitation method for the Hetero-EF treatment of amaranth food dye solution at strong alkaline conditions (pH 13.4) in a three-electrode cell that consists of GDE as working electrode and Pt and Ag/AgCl as counter and reference electrodes, respectively. The degradation and mineralization of the azo dye was solely by surface catalyzed process without contribution from homogeneous catalysis since the catalyst is insoluble at the working pH. Almost complete color removal and degradation efficiency (98%) and high mineralization efficiency (70%) was achieved after 90 min of treatment at 0.15 mM dosages and -1.1 V applied voltage.

Similarly, Zhou's group [135–137] have studied Fe-C modified by polytetrafluoroethylene (PTFE) as solid catalyst for Hetero-EF degradation of 2,4-dichlorophenol (2,4-DCP) at circumneutral pH with much emphasis on the influence of operating factors on degradation and mineralization of the pollutant, mechanism of degradation and degradation pathway. The catalytic activity of the Fe-C was well maintained after PTFE coating with much lower iron leaching; and the degradation efficiency of 2,4-DCP exceeded 95% within 120 min of treatment at current intensity of 100 mA, initial pH 6.7 and 6 g L<sup>-1</sup> catalyst dosage. A synergistic effect between anodic oxidation at the surface of the Ti/RuO<sub>2</sub>-IrO<sub>2</sub> and heterogeneous catalysis on the single Fe-C was observed for the degradation and mineralization of the 2,4-DCP (Fig. 8). The catalytic activity of PTFE modified Fe-C was highly stable and there was only negligible reduction in 2,4-DCP degradation efficiency over 15 cycles of consecutive runs with relatively low iron leaching ratio. Meanwhile, Ramírez et al. [138] utilized Fe – supported on Nafion membrane and ion-exchange amberlite and purolite resin as a catalyst in PEF process for degradation of aqueous orange-II dye solution. While up to 60% TOC removal was achieved under experimental conditions employed, the Fe was relatively fixed on the supports with

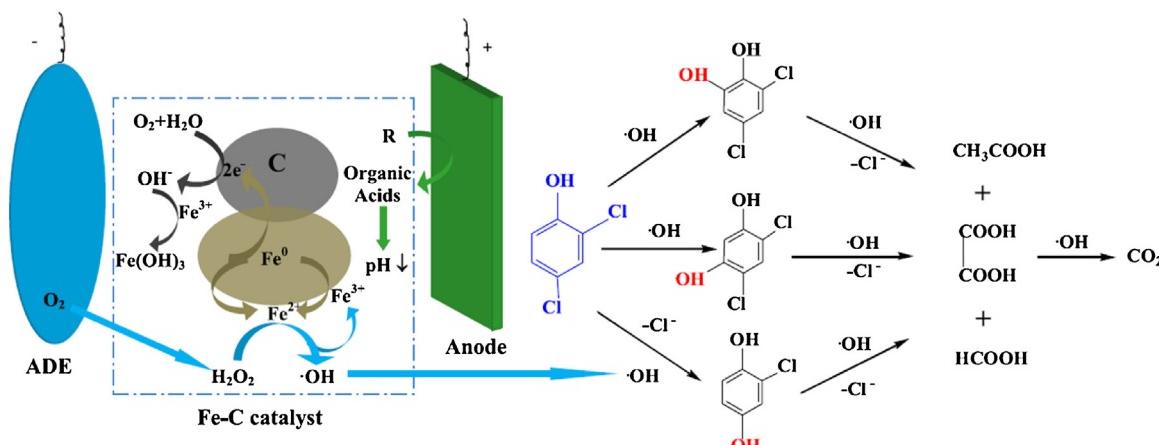
limited desorption.

Some studies have utilized solid Fe-containing compound in bioelectrochemical system/bioelectro-Fenton technology (BES/BEF) using microbial fuel cells (MFCs) [139,140]. In MFC, the biooxidation of organic substrate in the anode chamber by microorganisms produces electrons that are transfer via external circuit to the cathode, where it reduces electron acceptor mostly oxygen to  $H_2O_2$  [141–143]. The flow electrons produced electricity in the circuit due to drop in potential difference (Fig. 9). In essence, MFC converts chemical energy of organic substrate to electrical energy [144–146]. By addition of suitable iron source in the cathodic chamber of MFC, the produced  $H_2O_2$  can be catalytically activated to  $\cdot OH$  in a process called bioelectro-Fenton process (BEF) (Fig. 9) [147–149], thus utilizing the produced electricity to driven electrochemical system. Several studies have reported efficient mineralization of biorefractory organics in the cathode chamber of MFCs using BEF along with concurrent production of electricity.

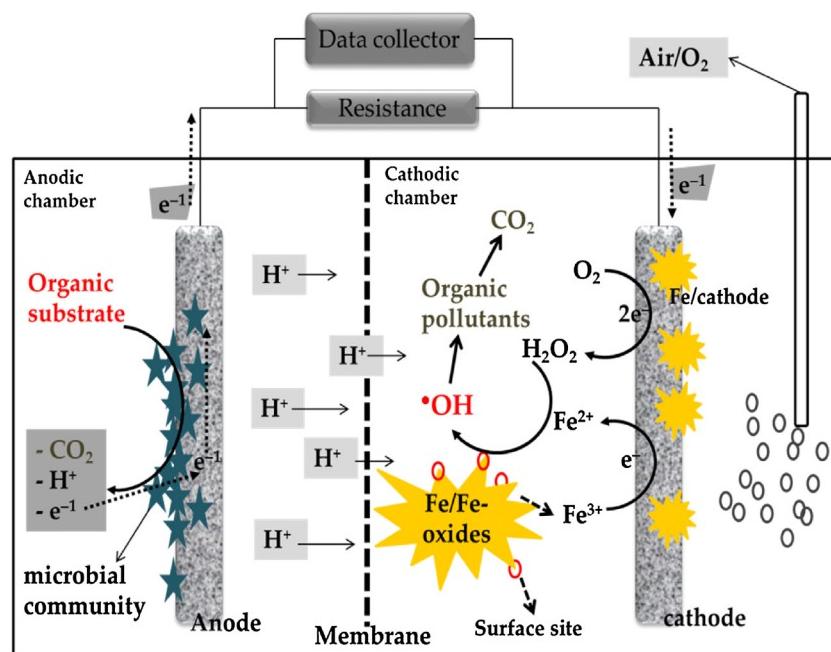
For instance, efficient removal of p-NP was reported by Tao et al. [139] in BEF using a dual chamber MFC with continuous injection of limonite ( $\alpha$ -FeOOH) powder into the cathode chamber as main source of iron dosage. Up to 96% of p-NP (0.25 mM) was removed in 6 h at optimal conditions and a limonite dosage of 112 mg per 50 mL of p-NP (0.25 mM) was found to sustained 7 cycles of BEF operation with p-NP removal efficiency > 94%. The mechanism of degradation of p-NP was by  $\cdot OH$  generated from catalytic decomposition of  $H_2O_2$  electro-generated at the carbon-felt cathode by homogeneous  $Fe^{2+}$  released into the bulk via partial dissolution of  $\alpha$ -FeOOH. Other studies related to Hetero-EF with iron/iron-containing nanoparticles and supported iron catalysts including BES/BEF are summarized in Table 3.

## 6. Heterogeneous electro-Fenton with Fe-functionalized cathodic electrodes

Fe-functionalized cathodic materials have been recently developed for application in heterogeneous electrocatalytic oxidation of refractory organic pollutants. In this context, the functionalized material serves dual purpose of electrode as well as the catalyst source in Hetero-EF system. In many cases, the catalysts are impregnated or loaded on materials with higher capacity to generate  $H_2O_2$ , such as active carbon/fiber, carbon-felt, graphite felt, and recently carbon aerogel. The catalytic performance in most cases is due to combination of both homogeneous oxidations in the bulk of the solution because of leaching of the catalyst and heterogeneous oxidation at the surface of the cathode at low pH values, whereas surface catalyzed process is predominant as pH increases (as explained in Section 3). However, the properties of the Fe-functionalized cathodic material especially the chemical stability in acidic solution play a key role in determine the contribution of the



**Fig. 8.** Proposed mechanism and degradation pathway of 2,4-DCP during the Hetero-EF treatment using Fe-C catalyst.  
Reprinted with the permission of Ref. [136].



**Fig. 9.** Microbial fuel cell-bioelectrochemical system (bioelectro-Fenton process) for the concurrent generation of electricity and heterogeneous EF treatment of organic pollutants.

Adopted from Ref. [139] with modification.

homogeneous EF in the overall mineralization of organic pollutants during Hetero-EF process. Additionally, the efficiency, stability and reusability of the catalyst impregnated electrodes/functionalized cathode are largely affected by the technique by which the catalyst is grafted onto the carbon matrix. The technique used controls the adhesion and mechanical wearing of the catalyst from cathode matrix. Several Fe-functionalized cathodic materials have been reported in literature with widely varying properties and synthesis/preparation techniques/routes, as such there is no consensus or generalized method to obtain the functionalized cathodic materials. However, based on the existing literature, these functionalized cathode materials can be broadly grouped into three classes according to the nature of the bulk material on which the Fe/Fe-containing compounds is loaded. These groups are: Fe-supported Fe-containing particle electrodes, Fe/Fe-containing compound modified carbonaceous cathode and Fe/Fe-transition metals carbon-aerogel and are discussed vividly in the next three sections.

#### 6.1. Fe-particle electrodes

Several studies have reported the use of 3D Fe-containing particle electrodes for heterogeneous electrochemical treatment of refractory organic pollutants. In most cases, the particle electrodes with high activity and stability are packed in between the anode and cathode of electrochemical cell for the degradation of the pollutants. The particle electrodes have been also demonstrated to enhance the conductivity of the solution and the mass transfer of substances during electrolysis [171]. Fe/Fe-compounds supported on mesoporous materials especially clay minerals are the most studied particle electrodes reported in literature, majorly because clay materials are largely abundant and inexpensive as a support material. Liu and co-workers [171] studied Fe-Ni foam particle electrodes for 3D EF treatment of RhB solution using Ti/RuO<sub>2</sub>-IrO<sub>2</sub> and activated carbon as anode and cathode, respectively. The 3D EF system was able to achieve higher RhB removal efficiency (99%) compared to analogous electrochemical system (without Fe-Ni foam) (33%) and EF system (13%) at neutral pH conditions in 30 min. The enhanced degradation efficiency was attributed to the production of more ·OH in the 3D EF system because the Ni-foam particle

electrodes could activate molecular oxygen to produce (O<sub>2</sub>·)<sup>-</sup> via a single electron transfer to subsequently generate more H<sub>2</sub>O<sub>2</sub> and in turn ·OH. Synthetic RhB solution has been also treated by 3D EF using iron-slag/clay particle electrodes in a micro-electrolysis cell equipped with Pt anode and stainless steel cathode [172]. The particle electrodes with particle size 3–5 cm was prepared from pot milled steel slag powder mixed with clay and pore forming agent and calcinated at 1050 °C for 30 min. The 3D EF treatment of RhB solution with the iron-slag/clay particle electrodes could achieve 82.4% and 65.45% removal efficiency with or without the airflow in 60 min. Additionally, the particle electrodes was found to exhibited satisfactory cyclic performance over 8 cycle of reuse. A typical degradation scheme involving particle electrodes and removal efficiency of Fe-Cu allophane clay particle electrodes for the mineralization of phenol are shown in Fig. 10a and b respectively.

A Chinese group has also studied a neutral 3D EF system with various bentonite-based Fe particle electrodes for the degradation of phenol [80], Acid Orange II [174] and pulp and paper mill wastewater [175]. The group showed that at optimal condition and pH 6.24, Fe<sub>3</sub>O<sub>4</sub>-bentonite, Fe<sub>2</sub>O<sub>3</sub>-bentonite and Fe<sup>2+</sup>-bentonite could achieve 13.28%, 57.8% and 67.48% COD removal respectively after 4 h of treatment of phenol solution. Analysis of the Fe leaching behaviors from the particle electrodes during the degradation of phenol revealed that both homogeneous and heterogeneous EF reactions contributed to the degradation of the phenol. Similar results were reported for Fe-bentonite particle electrodes for the degradation of Orange II with COD removal and decolorization efficiency of 71.57% and 98.89%, respectively [174]. Other relevant studies on the application of Fe-particle electrodes for 3D heterogeneous EF degradation of organic pollutants are summarized in Table 4.

#### 6.2. Fe-functionalized carbonaceous cathode material

Fe-functionalized cathode based on carbonaceous materials are the most widely studied functionalized cathodic materials for Hetero-EF treatment of organic pollutants because of the high capacity of carbonaceous materials for the in-situ production of large quantities of H<sub>2</sub>O<sub>2</sub> (Fenton reagent) during electrolysis. Indeed, several studies and

**Table 3**  
Summary of some relevant studies on Hetero-EF system catalyzed by Fe/Fe-supported solid catalysts.

| catalyst  | pollutants                        | electrodes  | Technology operation conditions  | main results   |
|---|-----------------------------------|---|--|--|
| Iron rich sludge  | 1,4-dioxane                       | Ti/RuO <sub>2</sub> /SS                             | EF   | undivided glass stirred tank reactor connected to Peristaltic pumps; 1000 mL solution; $j = 2.8 \text{ A cm}^{-2}$ for 120 min; pH 2.0–3.0 |
| Fe-AB   | Lissamine green B Azure B         | Gr  | EF   | undivided cylindrical glass reactor; 150 mL solution; 14.19 V applied potential for 30 min; 8.69 g Fe-AB; pH 2.8                           |
| Imidaprifloripid  | BDD/Gr                            | EF  | airlift continuous flow reactor; 1500 mL solution; 115 g Fe-AB; 1.5 L·min <sup>-1</sup> air flow; 3 V constant voltage; pH 2   |  |
| Indole  | Pt/CF                             | EF/PEF  | undivided closed glass reactor; 250 mL solution; $j = 0.13 - 0.8 \text{ mA cm}^{-2}$ , 50–250 mg L <sup>-1</sup> Fe-AB; pH 3; 25 °C  |  |
| Reactive Black 5  | Gr                                | EF  | undivided glass reactor; 150 mL solution; 5.69 V constant voltage; 2.68 mM of Fe/AB beads; pH 2.24   |  |
| Mn-AB   | Reactive Black 5                  | Gr  | undivided cylindrical glass reactor; 150 mL solution; 5 V constant voltage; 6–14 g Mn-AB dosage; pH 2  |  |
| Mn-AB, Fe-AB, and Fe-AC   | Winery wastewater                 | BDD/Ni-foam   | undivided cylindrical glass reactor; 150 mL solution in 0.01 M Na <sub>2</sub> SO <sub>4</sub> ; 15 V constant voltage; 1 L min <sup>-1</sup> air flow; 8.7, 14.25 and 3 g of Fe-AB, Mn-AB and Fe-AC respectively; natural pH            |  |
| Iron oxide-allophane clay   | Atrazine                          | Pt/GC   | three electrode undivided glass reactor; 8 mL of 46 mM atrazine solution; -1.04 V constant voltage; pH 3–6; 25 °C  |  |
| Fe-sepiolite  | Reactive Black 5                  | BDD/Gr  | undivided reactor; 150 mL of 100 mg L <sup>-1</sup> Reactive Black 5 solution; 3 g Fe-sepiolite; 5 V constant voltage; pH 2  |  |
| Fe-Y zeolite/Alginate   | Imidaprifloripid and chlorpyrifos | BDD/Gr  | undivided reactor; 150 mL solution; 5 V constant voltage; air flow rate 11 L min <sup>-1</sup> ; 50–700 mg L <sup>-1</sup> Fe-Y zeolite; pH 3  |  |
| Fe <sub>3</sub> O <sub>4</sub> NPs  | RB 19                             | Pt/ACF  | undivided cylindrical glass reactor; 200 mL of 100–300 mg L <sup>-1</sup> of RB19 in 0.05 M Na <sub>2</sub> SO <sub>4</sub> solution; 1.0 g L <sup>-1</sup> Fe <sub>3</sub> O <sub>4</sub> NPs; $j = 3 \text{ mA cm}^{-2}$ and pH 3      |  |
| rGO-Fe <sub>3</sub> O <sub>4</sub>  | 4,6-dinitro-o-cresol (DNOC)       | Gr  | undivided cylindrical cell; 200 mL of 11.4 μg L <sup>-1</sup> of DNOC in 0.08 M Na <sub>2</sub> SO <sub>4</sub> solution; 1 g of Fe <sub>3</sub> O <sub>4</sub> ; $I = 0.025 \text{ A}$ ; O <sub>2</sub> flow of 40 mL min <sup>-1</sup> |  |
| Pd-Fe <sub>3</sub> O <sub>4</sub>   | phenol                            | Pt  | undivided reactor; 150 mL of 10 mg L <sup>-1</sup> solution; $I = 0.5 \text{ mA}$ ; O <sub>2</sub> flow rate of 40 mL min <sup>-1</sup> ; 30% wt rGO-Fe <sub>3</sub> O <sub>4</sub> ; pH 2   |  |
| Pd-Fe   | MTBE                              | Ti/TiO <sub>2</sub> -Ta <sub>2</sub> O <sub>5</sub> | undivided cell; 400 mL of 20 mg L <sup>-1</sup> solution; $1 \text{ g L}^{-1}$ Pd/Fe <sub>3</sub> O <sub>4</sub> ; $I = 50 \text{ mA}$ ; pH 3; 25 °C   |  |
| Fe-AC   | m-cresol                          | BDD/Ni-foam   | undivided glass reactor; 150 mL of 100 mg L <sup>-1</sup> m-cresol solution; 28 mg L <sup>-1</sup> Fe in Fe-AC; air flow rate of 1 L min <sup>-1</sup> ; 5 V constant voltage; pH 3  |  |
| α-Fe <sub>2</sub> O <sub>3</sub> and α-Fe <sub>2</sub> O <sub>3</sub> /TiO <sub>2</sub> NTs | Phenol                            | Ni/TiO <sub>2</sub> NTs                             | undivided glass reactor; 100 mL solution of 0.0 mg L <sup>-1</sup> phenol solution; 5 V constant voltage; pH 3   |  |
| CuO/γ-Al <sub>2</sub> O <sub>3</sub>  | Amaranth                          | Pt/AQS-PPY  | Undivided electrolytic cell; 200 mL of 80 g L <sup>-1</sup> amaranth in 0.1 M Na <sub>2</sub> SO <sub>4</sub> solution; 1.25 g L <sup>-1</sup> of CuO/γ-Al <sub>2</sub> O <sub>3</sub> ; 0.4 V cell voltage; pH 4.3                      |  |
| Fe scrap  | p-NP                              | CF  | divided glass reactor; 300 mL of 1 mM p-NP; 10 g of scrap iron; pH 2   |  |
| FeVO <sub>4</sub>   | Orange II (AO7)                   | C-cloth/CF  | divided glass reactor; 200 mL of 50 mg L <sup>-1</sup> of AO7 solution; 1 g of FeVO <sub>4</sub> powder; pH 3  |  |
| γ-FeOOH   | AO7                               | PPy-AQDS/CF   | divided glass reactor; 75 mL of 0.2 mM of AO7; 1 g L <sup>-1</sup> of γ-FeOOH; pH 7  |  |

(continued on next page)

Table 3 (continued)

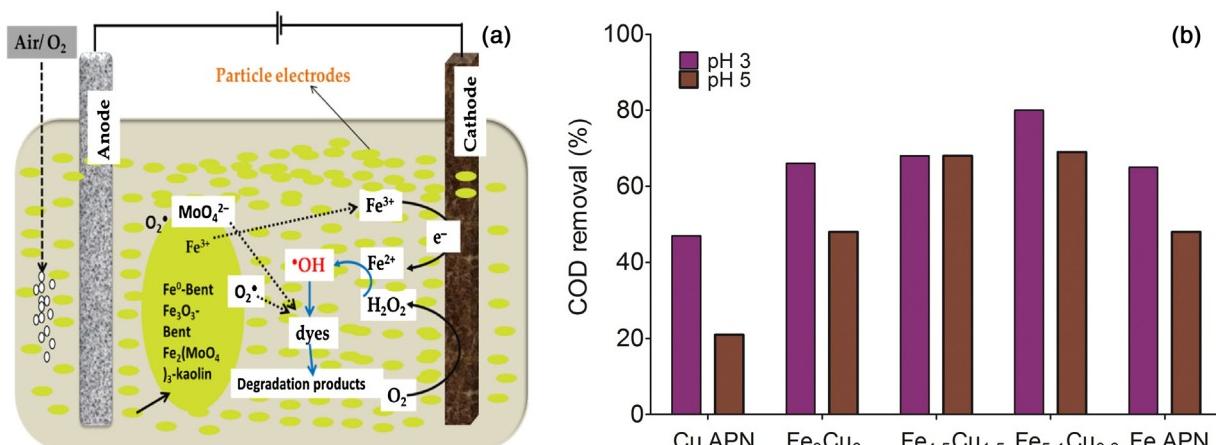
| catalyst                                     | pollutants          | electrodes | Technology operation conditions   | main results  |
|--|---------------------|------------|---|---|
| <b>Fe<sub>3</sub>O<sub>4</sub>-NPs</b>       | Acid red 14 (AR14)  | Gr/Gr-CNTs | EF  | Undivided glass reactor; 250 mL of either AR14 or AB92 in 4 g L <sup>-1</sup> Na <sub>2</sub> SO <sub>4</sub> solution  |
|  | Acid blue 92 (AB92) |            |   | 93.35% and 84.46% AR14 and AB92 removal efficiency at 0.18 A; pH 3 and 1 g L <sup>-1</sup> Fe <sub>3</sub> O <sub>4</sub> -NPs for AR14 and AB92 respectively [167] |
| Methylene blue (MB)                          | rGO-Gr              | EF         | –   | 98% and 99% removal for MB and AR14 respectively [168]  |
| AR14<br>Reactive black 5<br>Blue Sella solid | Gr                  | EF         | Undivided cylindrical reactor; 150 mL of dyes in 0.01 M Na <sub>2</sub> SO <sub>4</sub> ; 5 V constant voltage; air flow rate of 2 L min <sup>-1</sup>  | < 96% RB 5 removal after 120 min [169]  |
| Phenol                                       | SS                  | EF/PEF     | Undivided reactor; 1 L of 200 mg L <sup>-1</sup> phenol in 1 g L <sup>-1</sup> of Na <sub>2</sub> SO <sub>4</sub> ; 0.5 g L <sup>-1</sup> Fe° NPs; 500 g L <sup>-1</sup> H <sub>2</sub> O <sub>2</sub> ; pH 6.2 | 100% phenol removal in 30 min [170]   |
| <b>Fe-hydrogel</b>                           |                     |            |   |   |
| <b>Fe°-NPs</b>                               |                     |            |   |   |

Note: SS – stainless steel; Gr – graphite; CF – carbon-felt; GC – glassy carbon; AB – Alginic beads; rGO – reduced graphene oxide; MTBE – methyl *tert*-butyl ether; FCSW – iron contain sludge waste; GDE – gas diffusion electrode; AC – activated carbon, NTs – nanotubes, PPy-AQDS – polypyrrole-anthraquinone-2,6-disulfonate; CNTs- carbon nanoparticles.

substantial review works [4,79,183–185] have detailed the structural and physicochemical properties of most carbonaceous materials as electrodes for energy and environmental applications. They possess some distinguished characteristics such as good electronic conductivity and mechanical stability, excellent chemical stability, high surface areas and porosity which can provide abundant redox reaction sites and excellent electrolytic efficiency at relatively low cost [79,186–188]. Their high abundance in nature, inexpensive and easy accessibility make them most studied cathode materials in electrochemical wastewater treatment. Additionally, carbon is nontoxic and exhibits a high over-potential for H<sub>2</sub> evolution and low catalytic activity for H<sub>2</sub>O<sub>2</sub> decomposition [4,189]. Three dimensional carbonaceous materials, such as, activated carbon felt/fiber (ACF), graphite felt (Gr), carbon-PTFE O<sub>2</sub> diffusion (GDE) and carbon-felt (CF) are the most widely used material for the preparation of Fe-functionalized cathode due to their high ratio of surface area to volume, combined with high mechanical stability which is necessary for effective modification process [190]. Several modification methods at different experimental conditions have been reported for the preparation of Fe-functionalized carbonaceous cathode for the application in Hetero-EF treatment of organic pollutants. After modification process, the electrochemical activity of the carbon material could be significantly changed [19]. As stated earlier in Section 1, the Fe- functionalized carbonaceous materials acts as cathode or working electrode in the electrolysis cell on which dissolved oxygen is reduced to produce H<sub>2</sub>O<sub>2</sub> as well as iron source for the release of Fe-species required for the activation of H<sub>2</sub>O<sub>2</sub> to ·OH. Besides, the mechanism of the decomposition of H<sub>2</sub>O<sub>2</sub> to ·OH depends on the properties of the solid iron source loaded on the cathode and the working pH of the solution.

The functionalized cathode materials have been used both in conventional Hetero-EF as heterogeneous catalyst system and bioelectro-Fenton's system in MFCs for degradation of biorefractory organic pollutants. Especially worth nothing is the pioneer works which utilized Fe@Fe<sub>2</sub>O<sub>3</sub>/CNT as an effective oxygen-fed gas diffused cathode for a neutral EF system [63]. The Fe@Fe<sub>2</sub>O<sub>3</sub> nanowire was first synthesized by reaction between FeCl<sub>3</sub> and NaBH<sub>4</sub>. The Fe@Fe<sub>2</sub>O<sub>3</sub>/CNT cathode was prepared by mechanical rolling of paste made from a mixture of Fe@Fe<sub>2</sub>O<sub>3</sub>, CNT, and PTFE suspension in ethanol to form a 0.5 mm thin electrode. The prepared electrode was found to be efficient for H<sub>2</sub>O<sub>2</sub> electrogeneration; and the degradation of RhB with this electrode was 91.5% in 120 min at neutral pH conditions, demonstrating that the system was very promising for wastewater treatment. Subsequent studies by the same group investigated Fe@Fe<sub>2</sub>O<sub>3</sub>/ACF cathode because ACF can easily adsorb iron ions that can be reduced to Fe@Fe<sub>2</sub>O<sub>3</sub> by NaBH<sub>4</sub> [165]. It was found that the Hetero-EF system with Fe@Fe<sub>2</sub>O<sub>3</sub>/ACF cathode showed higher catalytic activity than EF systems catalyzed with commercial Fe° powders and ferrous ions (Fe<sup>2+</sup>) for degrading RhB. Since then, several other studies have utilized Fe- modified ACF/ AC for the Hetero-EF treatment of several pollutants such as m-cresol and RhB using iron-loaded AC [160] and methyl orange using Fe@Fe<sub>2</sub>O<sub>3</sub>/ACF cathode in bioelectro-Fenton's system with MFCs [191]. Excellent production of H<sub>2</sub>O<sub>2</sub> and high catalytic activity was also reported for electrochemically prepared iron-modified AC electrodes in Hetero-EF and Hetero-PEF treatment of synthetic methyl orange solution [113]. Almost total decolorization (96%) and TOC removal (88%) was attained during Hetero-EF treatment in 30 min of treatment, whereas complete decolorization (100%) and TOC removal (98%) was achieved in similar treatment time using Hetero-PEF process.

CF electrode has a high specific surface area that favors the fast generation of both Fenton's reagent (H<sub>2</sub>O<sub>2</sub> and Fe<sup>2+</sup>) and can be easily modified with Fe and/Fe-containing compounds for application in Hetero-EF system. Sklari et al. [33] investigated Fe-loaded CF composites prepared under oxidizing condition by immersing the CF in ethanolic solution of FeCl<sub>3</sub>.6H<sub>2</sub>O or reducing condition with continuous flow of N<sub>2</sub>. The Fe-CF prepared under reduced condition was found to have high stability and catalytic activity during Hetero-EF process,



**Fig. 10.** (a) Scheme for degrading organics by particle electrodes and (b) COD removal efficiency at pH 3 and 5 for the mineralization of 100 mL of  $5 \times 10^{-4}$  M phenol in 0.05 M Na<sub>2</sub>SO<sub>4</sub> by Fe-Cu allophane (APN) clay with different composition of Fe and Cu ( $\text{Fe}_{6-x}\text{Cu}_x$ ) at -0.6 V. Adopted from Refs. [173,82] for (a) and (b), respectively, with modification.

achieving diclofenac degradation and mineralization efficiency of 63.7% and 31.6%, respectively, at low applied potential of 1.0 V vs Ag/AgCl, pH 7 and 34 mg L<sup>-1</sup> initial diclofenac solution. Similar studies were reported by Brillas group [192] where CF/iron oxide air-diffused cathode prepared by Fe<sup>3+</sup> electrodeposition was utilized for the mineralization of malachite green dye in a Hetero-EF and UVA Hetero-PEF processes. It was observed that the oxidation of the malachite green at pH 3 was by hydroxyl radicals formed at the BDD anode surface from water oxidation and at the cathode or in the bulk from Fenton's reaction between the deposited or leached Fe<sup>2+</sup> and electrogenerated H<sub>2</sub>O<sub>2</sub> in both treatment, along with the photo-oxidation by UVA light in heterogeneous PEF. Complete decolorization of the dye was attained in both processes, whereas mineralization efficiency of 85% and 98% was achieved at 50 mg L<sup>-1</sup> malachite green, pH 3 and current density of 21.7 mA cm<sup>-2</sup> for Hetero-EF and UVA Hetero-PEF treatment respectively, after 6 h. Recently, we reported CoFe-layered double hydroxide (CoFe-LDH) modified CF as an efficient heterogeneous catalyst/cathode for mineralization of orange II [19]. The modified cathode synthesized by in-situ solvothermal process showed highly crystalline, porous and anisotropic CoFe LDH grown on CF (Fig. 11a–d).

Electrochemical characterization using cyclic voltammetry and EIS showed that the prepared cathode was highly stable at neutral pH conditions with almost zero percent Fe or Co leaching and good conductivity for electrochemical process. Excellent mineralization of orange II was obtained at all pH values studied and superior mineralization efficiency was always achieved in Hetero-EF with CoFe LDH/CF compared to conventional EF with added Fe<sup>2+</sup> and/or Co<sup>2+</sup> with relatively good reusability (Fig. 11e and f). The mineralization of orange II was via the formation several intermediates and carboxylic acids which were later mineralized to CO<sub>2</sub> (Fig. 12).

Other studies have reported Fe-modified graphite electrodes prepared with various iron sources and techniques for Hetero-EF treatment of different organic pollutants. Graphite electrodes have been extensively studied as suitable electrode (both anode and cathode) in electrochemical wastewater treatment owing to their excellent conductivity and mechanical integrity which can enhance their modification [185,193]. For instance, nanostructured iron oxide/graphite (FeOOH/graphite, Fe<sub>2</sub>O<sub>3</sub>/graphite and Fe<sub>3</sub>O<sub>4</sub>/graphite) electrodes fabricated from synthetic acid mine drainage was reported to have shown high stability and catalytic activity for the degradation of RhB in Hetero-EF system [194]. It was found that EF system using raw graphite could only achieve 30% RhB removal in 120 min whereas up to 62.5%, 94.5% and 95.6% was attained with FeOOH/graphite, Fe<sub>2</sub>O<sub>3</sub>/graphite and Fe<sub>3</sub>O<sub>4</sub>/graphite, respectively, at the same treatment time. More recently, Zhou group [46,116] investigated a novel roll-made GDE

loaded with trace transition metals (M/GDE, M=Cu, Ce, Mn, Fe, Co) as an effective cathode/catalyst for Hetero-EF (Hetero-EF-like) degradation of methyl orange. The prepared rolling-made GDE demonstrated a good catalytic activity and stability for H<sub>2</sub>O<sub>2</sub> production, with a maximum H<sub>2</sub>O<sub>2</sub> concentration of 595 mg L<sup>-1</sup> generated after 120 min and variation of less than 3.36% after 10 cycle of reuse. Among the cathodes studied, Co/GDE showed the highest activity at Co loading of 0.7 wt% with highly stable catalytic activity towards pH variation (pH 3–9). It was confirmed that the degradation of methyl orange was majorly by ·OH produced from the catalytic activation of H<sub>2</sub>O<sub>2</sub> in a Fenton or Fenton-like reaction. Table 5 summarizes some other relevant studies that have applied Fe-functionalized carbonaceous cathode materials for Hetero-EF/Hetero-PEF treatment of wastewater.

### 6.3. Fe-containing carbon-aerogel

Aerogel is a general term used to describe a class of material derived from organic, inorganic or hybrid molecular precursors that are normally prepared by sol-gel process and retain its three-dimensional and highly porous network after appropriate drying technology [208]. Aerogel was first developed in 1930's by S. Kistler using supercritical drying approach to extract pore-filling liquid of wet gels to obtain air filled solid structure with approximately same dimension as their initial wet gel [209,210]. Although, pioneer studies mainly focused on robust aerogels with different starting molecules, the subsequent studies investigated silica (SiO<sub>2</sub>) type aerogels [211–214]. Due to complex and intricate multistage synthesis procedures, aerogel as a porous material was abandoned and studies about its synthesis and applications were forgotten for over 30 years. However, different types of aerogels including inorganic (e.g. SiO<sub>2</sub> derived from alkoxysilanes, TiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub> and others) [211,215–218], organic (polyamide, polystyrene, polyurethane, etc.) [219,220], carbon (carbon, carbon nanotube, graphene) [221–224], semiconductor chalcogenide [225], natural based aerogels [226–228] and SiC aerogels [222,229–232] have been developed in the last decades due to advances in synthesis and drying technologies. In general aerogel are light material with overwhelming majority of its volume being air, which endows it with interesting physicochemical properties, such as high porosity and easy to modified or functionalized for excellent mass-transfer of reactants/substances [233–235].

Carbon aerogels (CAs) were extensively developed in early 90's with multi-facet properties and additional functionality such as mechanical strength, hydrophobicity and catalytic features for high performance applications [236–239]. They possess exclusive properties such as low density (~0.003–0.5 g cm<sup>-3</sup>), relatively high surface area

**Table 4**  
Summary of some relevant studies on the application of Fe/Fe-supported particle electrodes in Hetero-EF wastewater treatment.

| particulate electrodes   | pollutants    | electrodes              | technology | operation conditions   | main results  |
|--|---------------|-------------------------|------------|--|---|
| Fe-Mn – carbon black   | Nitrobenzene  | Pt// FMBO/ ACS/CB       | EF         | Open, undivided glass reactor; 400 mL of 100 mg L <sup>-1</sup> of NB in 0.05 M Na <sub>2</sub> SO <sub>4</sub> solution; O <sub>2</sub> flow rate of 0.3 L min <sup>-1</sup> ; 8.33 mg cm <sup>-2</sup> FMBO/AC loading; pH = 7 | 1.3 μM W <sup>-1</sup> cm <sup>-2</sup> of ·OH produced at pH 7; 80 ± 3% and 42 ± 7% NB removal for Pt//FMBO/AC/CB and 0.1 Fe <sup>2+</sup> EF respectively after 120 min [176] |
| Martite-particles  | Paraquat      | Gr/Pt                   | EF         | Undivided glass cell; 100 mL of 20 mg L <sup>-1</sup> paraquat in 0.05 M Na <sub>2</sub> SO <sub>4</sub> solution; 1 g L <sup>-1</sup> plasma modified martite catalyst; 300 mA applied current; pH 6                            | 85.78% and 41.03% paraquat removal efficiency in 150 min for plasma modified and unmodified martite particles [177]   |
| Fe-clay allo-phane   | Atrazine      | Fe-Clay-GC//Pt//Ag/AgCl | EF         | Undivided cell equipped with three electrodes; 30 mL of 45 mM atrazine in 90% 0.1 Na <sub>2</sub> SO <sub>4</sub> and 10% methanol solution; – 1.04 V constant voltage; pH 3–6   | 100% and 76% atrazine degradation efficiency attained at pH 3 and 6 respectively after 8 h treatment [81]   |
| Fe <sub>2</sub> (MoO <sub>4</sub> ) <sub>3</sub> ·kaolin 450 (FM-kaolin-450) | Methyl Orange | Gr/Gr                   | EF         | Undivided glass cell; 300 mL methyl orange solution in 0.05 M Na <sub>2</sub> SO <sub>4</sub> ; air flow rate of 1 L min <sup>-1</sup> ; pH 2 – 6.7  | 97% decoloration in 10 min and 92.48 COD removal in 60 min at pH 3 and current density of 68 mA cm <sup>-2</sup> [173]  |
| Fe-Cu allo-phane clay  | Phenol        | Fe-Cu/GC//Pt//Ag/AgCl   | EF         | Undivided cell equipped three electrodes; 100 mL of 0.5 mM phenol in 0.05 M Na <sub>2</sub> SO <sub>4</sub> solution; – 0.6 V; pH 3–5.5  | 100% phenol in 2 h and 80% COD removal at pH 3 in 4 h was attained with Fe-Cu allophane [82]  |
| Nano-Fe°/AC  | Methyl orange | Pt/graphite felt        | EF         | undivided cell; 130 mL of 60 mg/L solution; cathode potential – 0.65 V, pH = 3, O <sub>2</sub> flow rate 0.4 L/min   | 80% decolorization in 10 min, and 40% TOC removal after 2 h [178]   |
| Fe-Slag – clay particles   | RhB           | Pt/SS                   | EF         |  | 82.4% and 65.45 RhB removal efficiency with and without particulate respectively [172]  |

(continued on next page)

Table 4 (continued)

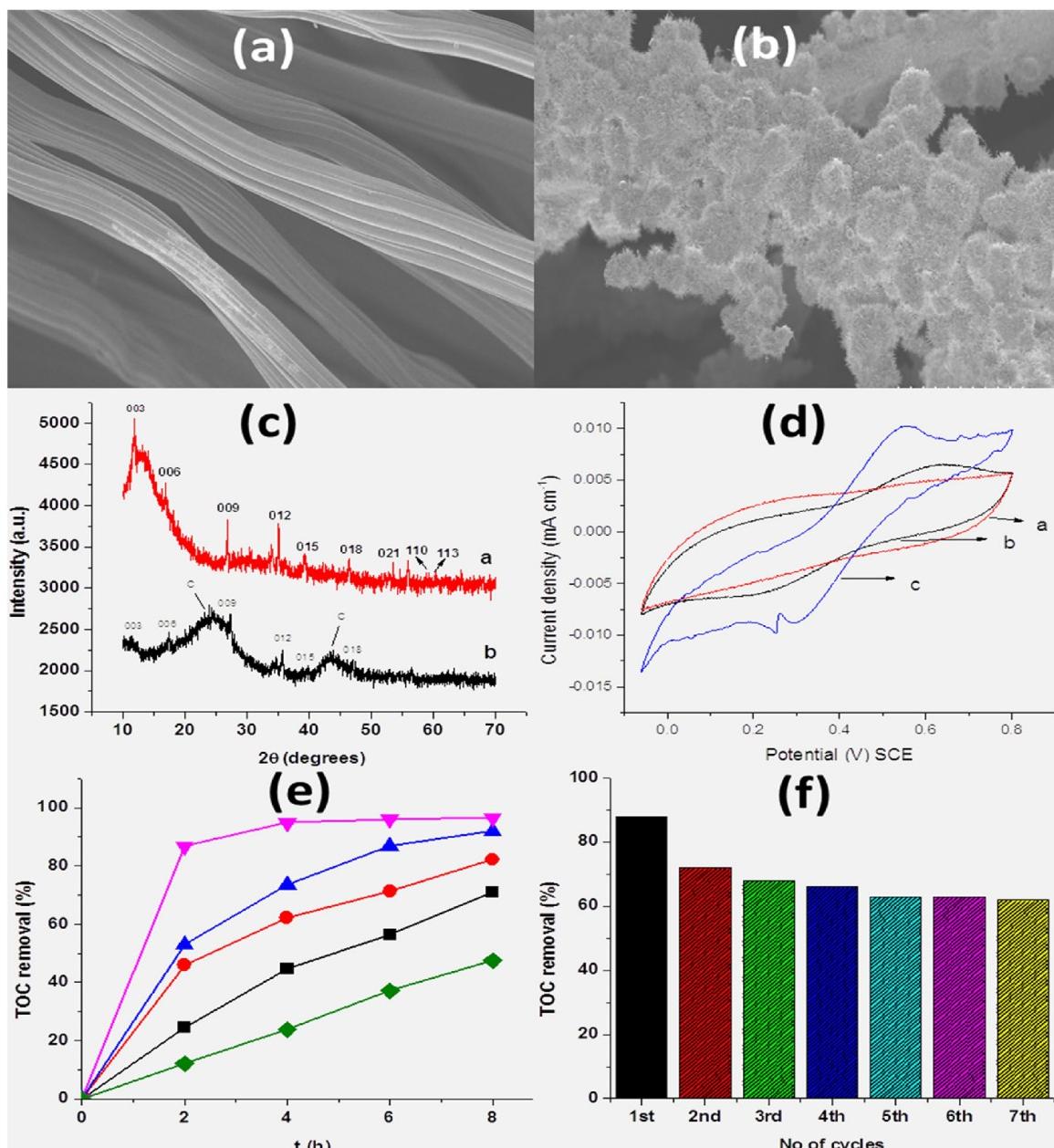
| particulate electrodes                       | pollutants                         | electrodes               | technology | operation conditions  | main results   |
|--|------------------------------------|--------------------------|------------|---|--|
| SAC-Fe or Fe <sub>3</sub> O <sub>4</sub> NPs | Coal gasification wastewater (CGW) | Tl/SnO <sub>2</sub> /ACF | EF         | Undivided cell; 1 L of CGW containing 173.3 mg L <sup>-1</sup> COD and 48.3 mg L <sup>-1</sup> total phenol; 5.0 g L <sup>-1</sup> SAC-Fe and 1.07 g L <sup>-1</sup> Fe <sub>3</sub> O <sub>4</sub> NPs; air flow rate of 4 L min <sup>-1</sup> ; pH = 6.8  | 78.1% and 37.1% COD removal with SAC-Fe and Fe <sub>3</sub> O <sub>4</sub> NPs respectively in 2 h [179] |
| CTAB-bent/ OH-Al-CTAB-bent                   | Paper and pulp mill wastewater     | SS/SS                    | EF         | Undivided tank reactor; wastewater contain 256 mg L <sup>-1</sup> COD and UV <sub>254</sub> 4.183 cm <sup>-1</sup> ; working volume of 500 mL; air flow rate of 2.5 L min <sup>-1</sup> ; applied current of 0–3 A  | 84.3 % and 93% COD and color removal efficiency respectively [175]                                       |
| Fe-bentonite (Fe-bent)                       | Orange II                          | Gr/Gr                    | EF         | Undivided glass reactor; 400 mL of 100 mg L <sup>-1</sup> Orange II in 0.05 M Na <sub>2</sub> SO <sub>4</sub> solution; 14.29 nA cm <sup>-2</sup> current density; 0.5 g PEs; pH 6.4  | 98.89% and 71.75% decolorization and COD removal efficiency after 1 h of treatment [174]                 |
| α and γ-FeOOH                                | RhB                                | AQ/rGO//Pt/Ag/AgCl       | EF         | Divided glass cell with cation exchange membrane separator; 0.01 M NaClO <sub>4</sub> as anolyte; 200 mL of 10 mg L <sup>-1</sup> RhB in 0.5 M Na <sub>2</sub> SO <sub>4</sub> or MgSO <sub>4</sub> catholyte; 100 g L <sup>-1</sup> of PEs; Oxygen flow rate of 0.6 L min <sup>-1</sup> ; – 0.5 V constant voltage | 100% RhB removal in 120 min [30]   |
| Pd-Fe/Ni-foam                                | DMZ                                | Pt/Pt                    | EF         |   | 96.5% DMZ removal achieved in 60 min with Pd-Fe/Ni-foam PEs [180]  |

(continued on next page)

**Table 4 (continued)**

| particulate electrodes              | pollutants | electrodes            | technology | operation conditions   | main results  |
|-------------------------------------|------------|-----------------------|------------|--|---|
| AuPd/Fe <sub>3</sub> O <sub>4</sub> | BMIM       | DSA                   | EF         | Undivided reactor;<br>400 mL of<br>50 mg L <sup>-1</sup> DMZ in<br>5 g L <sup>-1</sup> Na <sub>2</sub> SO <sub>4</sub><br>solution; air flow<br>rate of 1 L min <sup>-1</sup> ;<br>12.5 g L <sup>-1</sup> of PEs;<br>current density of<br>31 mA cm <sup>-2</sup> ; pH 3 | 100% removal of 10 mM BMIM in less than 40 min [181]                  |
| FCSW PE                             | p-NP       | PbO <sub>2</sub> /GDE | EF         | Undivided reactor;<br>150 mL of<br>BMIM containing<br>2.13 g Na <sub>2</sub> SO <sub>4</sub> and<br>1.5 g of AuPd/<br>Fe <sub>3</sub> O <sub>4</sub> ; applied<br>current of 300 mA;<br>pH 3   | 94.31% p-NP removal in 60 min and 78.96% TOC removal in 180 min [182] |
|                                     |            |                       |            | 50 mg L <sup>-1</sup> p-NP in<br>0.05 M Na <sub>2</sub> SO <sub>4</sub><br>solution; air flow<br>rate of 0.2 L min <sup>-1</sup><br>3 g L <sup>-1</sup> of FCSW<br>PEs; current density<br>3 mA cm <sup>-2</sup> ; pH 3;   |   |

Note: FMBO – Fe-Mn binary oxide; ACS – activated charcoal; CB – carbon black; SS – stainless steel; ACF – activated carbon felt; AQ – anthraquinone; DSA – dimensional stable anode; SAC – sludge derived activated carbon; BMIM – 1-butyl-3-methylimidazolium hexafluorophosphate; GDE – gas diffuse electrode; FCSW – fluffy clump steel wire; PE<sub>S</sub> – particle electrodes.

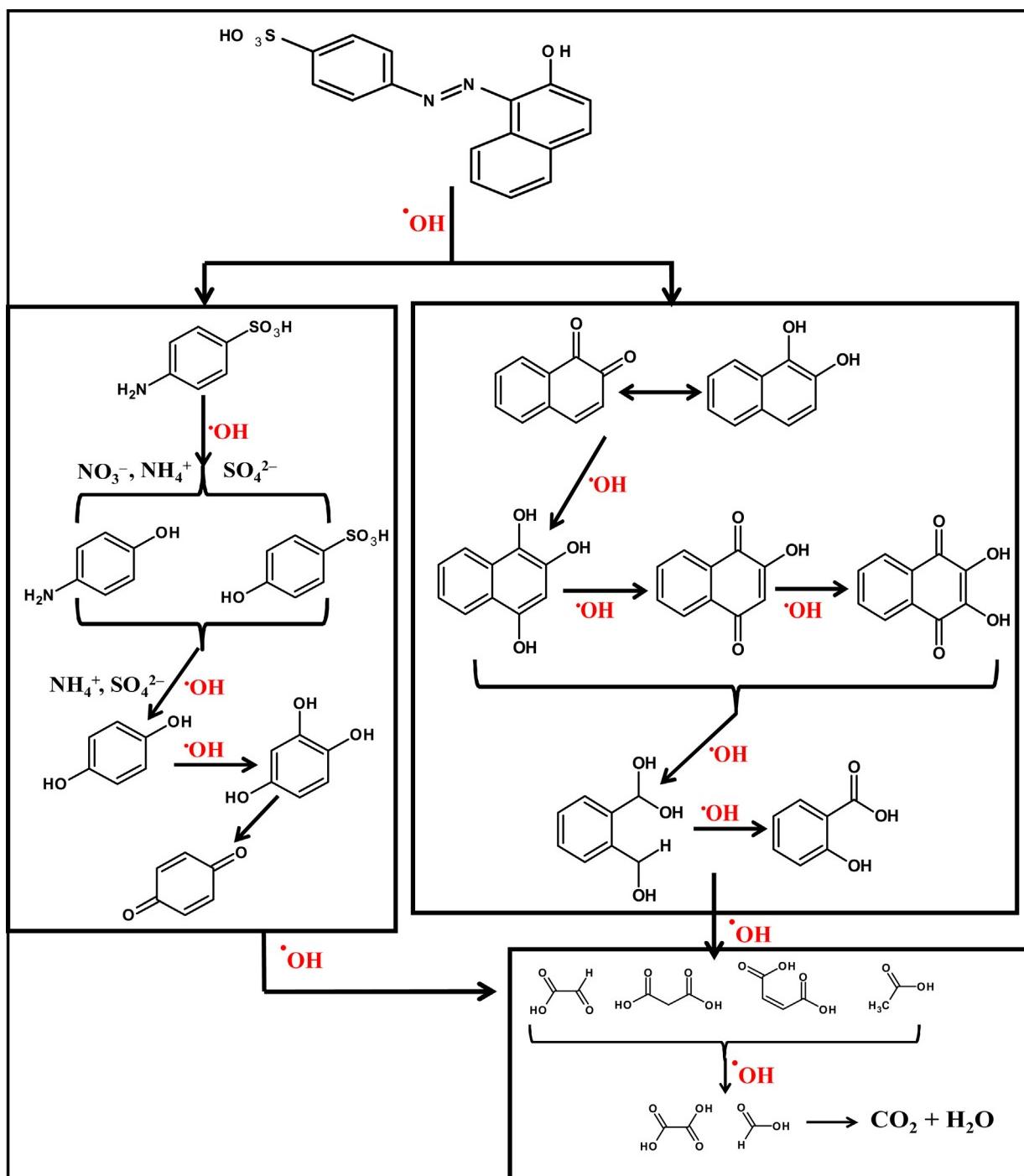


**Fig. 11.** SEM image of (a) raw CF and (b) CoFe-LDH/CF; (c) X-ray diffraction pattern of (a) CoFe-LDH powder and (b) CoFe-LDH/CF; (d) Cyclic voltammetry of CoFe-LDH/CF performed in 50 mM Na<sub>2</sub>SO<sub>4</sub> at (a) pH 5.83, (b) pH 3 and (d) pH 2; (e) comparison of TOC removal efficiency of (●) 0.2 mM Co<sup>2+</sup>, (■) 0.2 mM Fe<sup>2+</sup>, (●) 0.2 mM (Fe<sup>2+</sup> + Co<sup>2+</sup>) (1:1), (▲) 0.2 mM (Fe<sup>2+</sup> + Co<sup>2+</sup>) (2:1) and (▼) CoFe-LDH/CF during the mineralization of 150 mL of 0.1 mM AO<sub>7</sub> solution in 0.05 M Na<sub>2</sub>SO<sub>4</sub> at pH 3 and applied current of -40 mA using Pt anode; and (f) TOC removal efficiency with number of cycle using CoFe-LDH/CF at similar conditions as (e). Reprinted with the permission of Ref. [19].

(~500–1200 m<sup>2</sup> g<sup>-1</sup>), high porosity (~88–99.8%) with tunable surface chemistry combined with ability of being processed into a variety of morphologies and sizes to suit different applications [240,241]. CAs is a hybrid aerogels which could well combine advantages of several materials to achieve specific function. Among other properties, CAs is characterized by high electrical conductivities and good corrosion resistance especially under the strong oxidizing conditions [222,242–244]. The mechanical robustness and thermal stability of CAs could be tremendously enhanced when hybridized with iron aerogel, which is known for its strong mechanical and thermal strength. This type of hybrid aerogel, containing carbon and iron network, has been developed as a prospective candidate for catalytic applications [32,236,245]. Indeed, several studies have demonstrated the suitability of this material as Fe-functionalized cathodic material for Hetero-EF

and Hetero-PEF processes, in the last four years.

CAs is prepared by wet chemical synthesis approach, sol-gel reaction, but through different starting precursors, operating and provision requirement [214]. The complete steps involved in CAs preparation include sol-gel formation, solvent exchange, ambient pressure drying and pyrolysis (Fig. 13) [246–248]. Firstly, mixture solutions of precursors, water and catalysts are transformed into highly dispersed solution of colloidal primary particles or monomers via hydrolysis and polycondensation reactions to form sols. The colloidal particles of the sol can connect to one another to form three-dimensional and interconnected network upon addition of chemical cross-linker or by changing the conditions of reaction (i.e. pH, temperature) [249–252]. The formation of the porous three dimensional networks is the most critical and determinant aspect of aerogel [209]. The pore-filling solvent of the



**Fig. 12.** Reaction mechanism for complete degradation of orange II by  $\cdot\text{OH}$ . Reprinted with the permission from Ref. [19].

wet gel is exchanged with volatile solvent to form the highly porous network. To prepare functionalized CAs (i.e. Fe-functionalized CAs), iron/transition metal containing compounds are added to the homogeneous precursor solution prior to the formation of sol [251–255]. The wet gel is subjected to curing and ageing because the chemical reactions are not finished with gel formation [256]. In fact during the ageing, the reactive species such as  $-\text{OH}$  or unreacted monomers contained in the gelation solvent inside the pores are condensed onto the network. The curing or ageing process is commonly performed by soaking the gel in the initial sol or suitable solvent under controlled conditions (pH, time and temperature) for long period ranging from hours to days [212,246,256,257]. The 3D networks of the gel is strengthening and

coarsening and there are changes in textural properties of the gel such as pore size, porosity and surface area during the ageing process [258–262]. Drying the gel without collapsing the original porous 3D structure is a critical step in aerogel preparation process [262–265]. Supercritical drying (using alcohol, acetone, or  $\text{CO}_2$ ) is the most popular conventional method for drying wet gel, but it requires reactors withstanding high pressure, which greatly increase the production cost [266,267]. Ambient pressure drying and freeze-drying are some of other prominent drying method reported in literature, however, most studies on Fe-functionalized CAs utilized ambient pressure drying, which is easy and inexpensive [268–270]. The final step of CAs preparation is carbonization of the dry gel at high temperature ( $> 600^{\circ}\text{C}$ )

**Table 5**  
Summary of some relevant studies on application of Fe/transition metals modified carbonaceous cathode for Hetero-EF wastewater treatment.

| Functionalized cathode   | Preparation method   | pollutant                    | technology | Operation conditions  | Main results  |
|--|--|------------------------------|------------|---|---|
| Fe/AC  | Electrochemically, using three electrode cell with AC suspended in $\text{H}_2\text{SO}_4$ and addition of $\text{FeCl}_3$ in drops  | MO                           | EF/PEF     | Undivided glass cell equipped with three electrodes; 25 mL of 10 ppm of MO solution; – 900 mV cathode potential; pH 3; 25 °C  | EF - 96% decolorization and 88% TOC removal in 30 min [113]                                       |
| Fe <sub>3</sub> O <sub>4</sub> /GDE  | Fe <sub>3</sub> O <sub>4</sub> /AC was prepared by precipitation method; then mixed with PTFE, ethanol and $\text{Na}_2\text{SO}_4$ before forming under in hydraulic machine  | Tetracycline (TTC)           | EF         | Undivided glass cell; 100 mL of 50 mg L <sup>-1</sup> TTC in 0.05 M $\text{Na}_2\text{SO}_4$ solution; – 0.8 V potential vs SCE; pH 3   | 94.2% TTC removal in 100 min [195]  |
| Fe <sub>2</sub> O <sub>3</sub> /C/graphite membrane cathode                              | i) pretreatment of Gr membrane; ii) deposition of active layer containing carbon black (CB) and Fe<br>iii) deposition of reductive and protective layer using CB and PTFE<br>oxidizing condition - soaking of CF in $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ and dried or reducing condition - passing N <sub>2</sub> into solution prior soaking | Flutriafol                   | EF         | Flow reactor; working volume of 54.84 cm <sup>3</sup> at 22.9 L m <sup>-2</sup> h <sup>-1</sup> flux; 100 mg L <sup>-1</sup> of flutriafol in 0.05 M $\text{Na}_2\text{SO}_4$ ; current density of 13 mA cm <sup>-2</sup> ; CB/Fe of 6.2; 1; pH 6.7 | 79.6% flutriafol removal [196]  |
| $\gamma$ -Fe <sub>2</sub> O <sub>3</sub> /Fe <sub>3</sub> O <sub>4</sub> /CF (Fe-NPs/CF) | oxidizing condition - soaking of CF in $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ and dried or reducing condition - passing N <sub>2</sub> into solution prior soaking  | Diclofenac                   | EF         | Flow reactor with 3 pair of anode/cathode; flow rate 40 L h <sup>-1</sup> ; V = 2 V per anode/cathode;  | 85% and 36% diclofenac and TOC removal efficiency respectively [197]                              |
| FeC <sub>x</sub> /N-doped carbon fiber (FeC <sub>x</sub> /NCNFs)                         | FeC <sub>x</sub> was prepared by electrospinning using iron (III) acetylacetone, N,N-dimethylformamide and polyacrylonitrile solution  | Dimethylarsinate (MDA)       | EF         | Undivided cell, 100 mL of 5 mg L <sup>-1</sup> DMA in 0.05 M $\text{Na}_2\text{SO}_4$ solution; O <sub>2</sub> flow rate of 50 mL min <sup>-1</sup> ; applied current of 0.15 A; pH 3   | 96% DMA removal in 6 h with residual As (V) concentration less than 0.01 mg L <sup>-1</sup> [198] |
| Fe <sub>3</sub> O <sub>4</sub> /graphite felt (Fe <sub>3</sub> O <sub>4</sub> /Gr)       | MFC treatment of acid mine drainage using Gr anode; after operation, Gr anode was remove and calcined<br>Co-precipitation of pre-hydrolyzed ferric and ferrous salt in the presence of QEG   | RhB                          | EF         | Undivided reactor; 175 mL of 50 mg L <sup>-1</sup> RhB in 50 mM $\text{Na}_2\text{SO}_4$ solution; O <sub>2</sub> flow rate = 1.5 L min <sup>-1</sup> ; pH 6.8  | 100% decolorization and mineralization in 10 and 70 h respectively [199]                          |
| QEG/Fe <sub>3</sub> O <sub>4</sub> composite   |  | Bisphenol                    | EF         | Undivided cell; 60 mL of 5 mg L <sup>-1</sup> bisphenol in 0.05 M $\text{Na}_2\text{SO}_4$ solution; air flow rate = 1 L min <sup>-1</sup> ; V = –1.2 V; pH 3   | Complete bisphenol removal in 90 min [200]  |
| Fe <sub>2</sub> O <sub>3</sub> /Gr   | Precipitation using $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ and NaBH <sub>4</sub> solution added in drop   | Alcohol wastewater           | EF         | Undivided glass reactor; 250 mL of wastewater; applied current of 51.54 mA; pH 2.84   | 66.15% COD removal in 69.29 min [42]  |
| Fe@Fe <sub>2</sub> O <sub>3</sub> /ACF   | Precipitation using $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ and NaBH <sub>4</sub> solutions  | MO                           | BES-EF     | Divided reactor (MFC); 500 mL of 5 mg L <sup>-1</sup> of MO in 0.05 M $\text{Na}_2\text{SO}_4$ ; O <sub>2</sub> flow rate of 750 mL min <sup>-1</sup> ; pH 3  | 73.9%–86.7% MO removal efficiency for eight successful cycle [191]                                |
| Fe@Fe <sub>2</sub> O <sub>3</sub> /CF  | Precipitation using $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ and NaBH <sub>4</sub> solutions  | RhB                          | BES-EF     | Divided reactor (MFC); 75 mL of 15 mg L <sup>-1</sup> of RhB solution; pH 3   | 95% and 90% RhB decoloration and TOC removal respectively in 12 h [201]                           |
|  |  | Swine wastewater             | BES-EF     | Divided flow reactor at 3.1 or 1.24 L day <sup>-1</sup> with organic loading 1.1 and 4.6 g COD L <sup>-1</sup> day <sup>-1</sup> ; pH 3   | 62.2%–95.7% COD removal efficiency [141]  |
|  | E2 and EE2   |                              | BES-EF     | Divided reactor; 75 mL of 20 mg L <sup>-1</sup> each of E2 and EE2 in 0.1 M NaCl; air flow rate of 100 mL min <sup>-1</sup> ; pH 3  | 81% and 56% removal for E2 and EE2 after 10 h [202]   |
|  | Precipitation using $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ and NaBH <sub>4</sub> solutions  | Triphenyltin chloride (TTCl) | BES-EF     | Divided reactor; 30 mL of 100 mg L <sup>-1</sup> TTCl solution; air flow rate of 100 mL min <sup>-1</sup> ; pH 3; 30 °C   | 78.32 ± 2.07% TTCl degradation efficiency at rate of 0.775 ± 0.021 h <sup>-1</sup> [203]          |
|  |  | Medicinal herb wastewater    | BES-EF     | Divided cell; 450 mL of wastewater; pH 3  | 84.02% COD removal [204]  |
| FeOOH/TiO <sub>2</sub> -GAC  | Sol-gel preparation of TiO <sub>2</sub> with addition of FeOOH/GAC   | Tetracycline                 | BES-EF     | Divided cell with MBR; 78.75 mL of tetracycline with continuous air flow  | 90% and 80% COD and NH <sub>4</sub> -N removal respectively [205]                                 |
| Pyrrhotite/Gr  | Grafting using conductive silver paste   | Landfill leachate            | BES-EF     | Divided cell; 250 mL of landfill leachate; pH 5.4   | 77% and 78% color and COD removal respectively [206]  |

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Table 5 (continued)

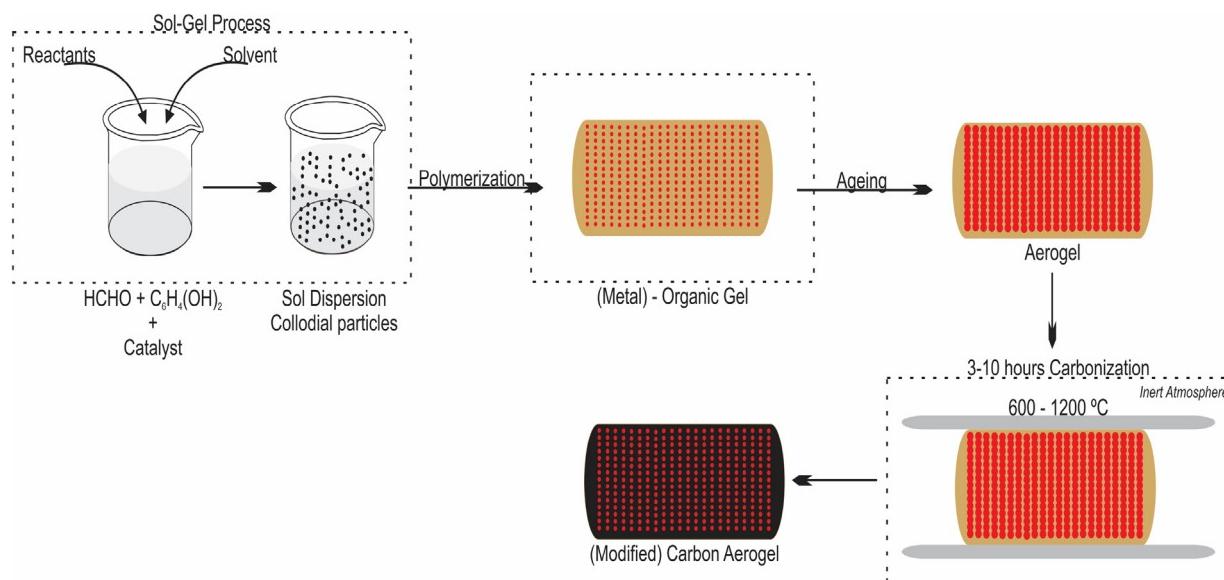
| Functionalized cathode | Preparation method   | pollutant   | technology | Operation conditions   | Main results  |
|------------------------|--|-------------|------------|--|---|
| CNT/ $\gamma$ -FeOOH   | Forming at high pressure using paste made from a mixture of CNT, $\gamma$ -FeOOH, PTFE and ethanol | Orange II   | BES-EF     | Divided cell; 75.6 mL of 0.1 mM orange II; pH 3  | 100% decolorization and mineralization efficiency [140]                           |
| Pd-Fe/Gro              | Photo-induced reduction  | 4-bisphenol | EF         | Divided cell; 150 mL of 100 mg L <sup>-1</sup> 4-bisphenol in 0.03 M Na <sub>2</sub> SO <sub>4</sub> solution; current density of 25 mA cm <sup>-2</sup> ; pH 7 and t = 60 min | 100% and 99.5% removal of 4-bisphenol in catholyte and anolyte respectively [121] |
| Fe-CHI/Ni AGF  Fe-CHI  | Deposition of Fe <sup>2+</sup> -CHI on Ni foam followed by fastening with elastic rope             | RhB         | EF         | Divided cell; 5 mg L <sup>-1</sup> in 0.05 M Na <sub>2</sub> SO <sub>4</sub> ; air flow of 0.1 m <sup>3</sup> min <sup>-1</sup> ; applied current of 10 mA; pH 6.2             | 93% degradation in 120 min [207]  |

Note: QEEG – Quinone-functionalized electrochemically exfoliated graphene; BES – bioelectrochemical system; Fe-CHI – Fe-chitosan.

and ambient pressure under an inert atmosphere of N<sub>2</sub> or Ar to decompose oxygen and hydrogen moieties in the polymeric chain and enriches the network with the pure carbon moieties [271,272]. The synthesis procedure for modified CAs preparation is presented in Fig. 13.

The earlier studies on the potential of CAs in electrochemical wastewater treatment utilized CA as particle electrodes for electrocatalytic degradation of RBRX dyes [273] and synthetic phenol wastewater [244]. The CA particle electrodes prepared by ambient pressure drying technique showed excellent degradation (~98%) of RBRX and phenol as well as high catalytic stability up to 20 cycles of reuse. Most studies on application of Fe – functionalized CAs cathode for 3D Hetero-EF/PEF system were conducted by Zhao group with focus on homogeneous Fe<sub>3</sub>O<sub>4</sub>@Fe<sub>2</sub>O<sub>3</sub> [45], ferrite [20], Fe<sub>3</sub>O<sub>4</sub>@C, and Fe-Cu [274] CAs. In all their studies, Fe-functionalized CAs was prepared by sol-gel formation, solvent exchange, ambient pressure drying and pyrolysis as described above and the prepared cathodes always exhibited good conductivity, high catalytic efficiency and distinguish stability. For example, Fe<sub>3</sub>O<sub>4</sub>@Fe<sub>2</sub>O<sub>3</sub> CAs composite cathode was reported to achieve excellent efficiency for the degradation of pesticide imidacloprid during Hetero-EF treatment in pH range of 3–9. Approximately 90% imidacloprid and TOC removal was attained in 30 and 60 min of treatment respectively, at current density of 10 mA cm<sup>-2</sup> and pH 3 [45]. The catalytic activity of Fe<sub>3</sub>O<sub>4</sub>@Fe<sub>2</sub>O<sub>3</sub> CAs was satisfactorily stable with pH as the change in TOC removal efficiency values was less than 3% for treatment performed between pH 3–pH 9. Similar results were obtained during the Hetero-EF treatment of an active ingredient of conventional fungicide metalaxyl with homogeneous ferrite CA [20]. The prepared ferrite CA was able to achieve 98% of TOC elimination in 4 h at pH 3 and stable catalytic activity over ten (10) cycles of reuse at pH 6, with less than 2% difference in TOC removal (Fig. 14). The same group reported similar behavior for continuous bulk ultradispersed Fe-Cu CA cathode during the Hetero-EF degradation of MB dye with high TOC removal achieved at wide range of pH values (pH 3–9) [97]. It was demonstrated that the COD of the treated real dyeing wastewater was below China's discharge standard after just 30 min of treatment with very low power consumption (0.34 k W h per ton of wastewater). In a related study [275], Fe-Cu embedded CA was reported to have achieved efficient TOC removal (88–99%) in 240 min during the Hetero-EF treatment of dimethyl phthalate, imidacloprid, bisphenol A and perfluorooctanoate. Successful decontamination of five sanitary sewages were also exhibited by the same cathode with the residual COD less than China national discharge standard (< 50 mg L<sup>-1</sup>) at low specific energy consumption. Similar results was achieved for the treatment of dimethyl phthalate (DMP) using highly ordered mesoporous Fe<sub>3</sub>O<sub>4</sub>@C CA with 95% and 65% DMP degradation and mineralization efficiency attained in 120 min respectively [274].

Fe-functionalized CA has also been studied as cathode material in Hetero-PEF process for the degradation of RhB and DMP using 2Fe/Co-CA [276] and imidacloprid using Fe<sub>2</sub>O<sub>3</sub> –CA [92]. 100% and 80% removal efficiency was obtained at 45 and 120 min for RhB and DMP respectively in solar Hetero-PEF treatment, whereas complete degradation of imidacloprid could be only reached in 180 min under similar solar Hetero-PEF treatment. Other studies have also reported high catalytic activity and stability for iron oxide-graphene/CNT – CA composite cathode for the Hetero-EF degradation of MB [32]. The authors showed that 99% removal efficiency of MB can be achieved in 60 min at pH 3 and applied current of 15 mA using 5% Fe containing graphene/CNT – CA. In all studies that involve Fe-functionalized CA composite cathode, two mechanisms was always proposed for the activation of H<sub>2</sub>O<sub>2</sub> to ·OH during the Hetero-EF process as described in Section 3, depending on pH of the treated solution. At acidic pH values, there was slight leaching of Fe and/or Cu/Co from the functionalized CA cathode into the solution, thus the activation of H<sub>2</sub>O<sub>2</sub> to ·OH is controlled by cycling of Fe<sup>3+</sup>/Fe<sup>2+</sup> and/or Cu<sup>2+</sup>/Cu<sup>+</sup>//Co<sup>3+</sup>/Co<sup>2+</sup> redox couple in the solution and at the surface of CA cathode. However



**Fig. 13.** Scheme for the synthesis of CAs.

Adapted from Ref. [20,208].

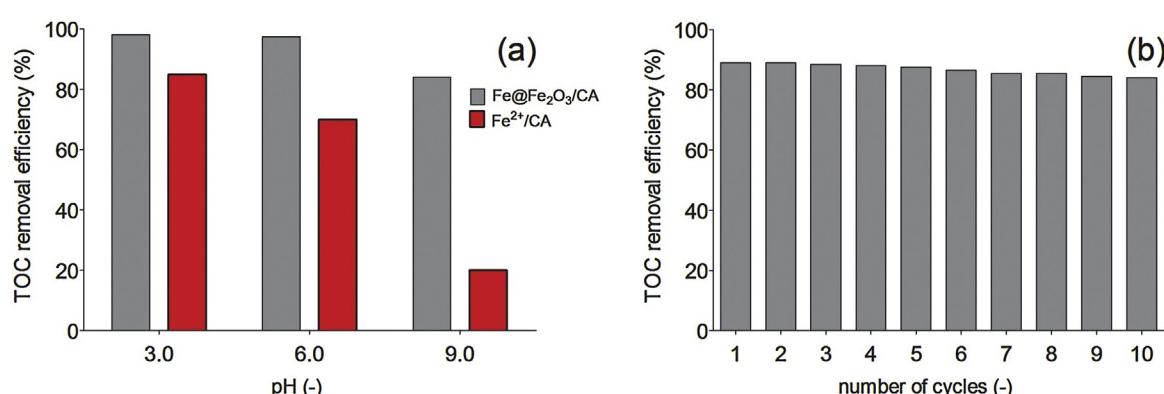
at neutral and alkaline pH values, only surface catalyzed activation should be predominant because Fe and/or Cu/Co are not soluble at such pH conditions. Besides, photo-assisted Hetero-EF usually gives better mineralization and current efficiency compared to analogous Hetero-EF, thanks photo-degradation of carboxylic complex as well as generation and regeneration of additional ·OH and Fe<sup>2+</sup> respectively from the photo excitation of Fe-complexes.

## 7. Challenges and future prospects

Some of the main challenges encountered in Hetero-EF/PEF are mostly related to the heterogeneous catalyst itself, especially supported catalyst and functionalized cathode used in Hetero-EF and Hetero-PEF system, though a cost-effective production of hydrogen peroxide on the cathode is essential [277,278]. Among these problems, catalyst fall-off from the support due to mechanical wearing in the solution and dissolution/excessive leaching of the catalyst at strong acidic pH are the most detrimental challenge that affects both catalytic stability and reusability efficiency of heterogeneous catalyst. Except in few cases like functionalized CAs, rolling made GDEs and some Fe-modified carbonaceous cathodes, excessive leaching or dissolution were usually observed when operating at strong acidic pH values (< pH 4), as such the overall electrolysis system is controlled by homogeneous catalysis by

recycling Fe<sup>3+</sup>/Fe<sup>2+</sup> redox couple. In this case, the efficiency of the electrochemical system usually depreciates significantly with increase in pH because the contribution of homogeneous EF diminishes with rise in pH conditions. Additionally, the mechanical wearing or fall-off of the catalyst from the support or cathode may increase with electrolysis time as the solution weakens the adhesive bond between the catalyst and the support regardless of operating pH values. This phenomenon was observed during Hetero-EF treatment of AO7 using solvothermal synthesized CoFe-LDH/CF cathode at pH 5.83, with mechanical fall off of the CoFe-LDH from the CF substrate after 6 cycles of 2 h repeated reuse due to the strong agitation of the solution and weakening of the bond between the CoFe-LDH and the CF [19]. The same thing could be indicated for Fe-loaded clay materials, ACF and iron sludge. However, this problem is limited or completely eliminated in functionalized CAs because the catalyst (Fe/Fe-compounds or Cu/Co) are not only embedded in the bulk of the CAs but also form the integral part of the 3D network of the CAs as explained in Section 6.3.

Agglomeration of the catalyst is another challenge that is commonly encountered in Hetero-EF and Hetero-PEF systems, especially with non-supported catalyst. Most synthetic non-supported heterogeneous catalysts such as pure Fe<sub>2</sub>O<sub>3</sub>, Fe<sub>3</sub>O<sub>4</sub> or Fe° or their doped/modified form are usually prepared and used as nanoparticles, as such there are usually tendency of agglomeration of these particles with treatment time,



**Fig. 14.** (a) comparison of TOC removal efficiency at different pH for Fe@Fe<sub>2</sub>O<sub>3</sub>/CA and CA with 1 mM L<sup>-1</sup> Fe<sup>2+</sup> during the treatment of 100 mL of 500 mg L<sup>-1</sup> metalaxyl solution in 0.1 M Na<sub>2</sub>SO<sub>4</sub> at 10 mA cm<sup>-2</sup> using BDD anode and (b) reusability of Fe@Fe<sub>2</sub>O<sub>3</sub>/CA during the 4 h a cycle at similar condition as (a). Reprinted with the permission of Ref. [20].

which reduces the effective surface area and active site of the catalyst and in turn the efficiency of the system. This is particularly the case of magnetic Fe-containing nanocatalyst like  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}^\circ$  where the nanoparticles not only attached to one another but also very difficult to agitate the electrolytic system, even though such system has an advantage of easy separation of the catalyst for possible reuse. More so, most synthetic supported or non-supported catalyst as well as Fe-functionalized cathode requires either multi-steps or complex preparation techniques which has limited most studies on Hetero-EF system to laboratory or pre-pilot scale. A typical example is functionalized CAs whose preparation involves at least four different non-related steps, thus makes the preparation route a bit complex, even though functionalized CAs remains one the most efficient heterogeneous catalyst/cathode based on literature.

Future studies in Hetero-EF and Hetero-PEF approaches should be tailored towards developing low-cost solid catalyst with improve stability in acidic pH, treatment of real wastewater, scale-up/pilot plant and flow-reactors based on these systems and in-situ spectroscopy studies of the  $\text{H}_2\text{O}_2$  activation mechanisms at the surface of the solid catalyst. It is important to enhance the stability of the solid catalyst at acidic pH values as studies have shown that most of the existing catalysts undergo significant leaching at strong acidic pH values, which make the system, behave like homogeneous EF and PEF processes. The economic cost and environmental impacts of both existing and future solid catalysts and functionalized cathodic materials should be considered in forthcoming studies. Previous studies on Hetero-EF has failed to address these key issues especially the environmental impact of the nanocatalysts on biotic component of the ecosystem of the receiving water bodies, where wastewaters are disposed after treatment. This information is crucial to engineers and regulatory agencies/bodies in charge of adapting new technologies. Besides, more studies are still required on the application of Hetero-EF for the treatment of real wastewater with complete cost analysis because there is a significant difference in the behavior of real and synthetic wastewater during the electrochemical treatment. Real wastewaters are complex in composition and properties; as such their electrochemical treatment may behave differently in terms of efficiency and removal mechanisms when compared to synthetic wastewater. Both the  $\cdot\text{OH}$  scavenging effect of the inorganic ions and natural organic matters in the real wastewater as well as synergistic effect of the different organic pollutants on the efficiency of the Hetero-EF process require further studies.

The mechanisms of activation of  $\text{H}_2\text{O}_2$  to  $\cdot\text{OH}$  have not been extensive studied and no consensus on reactions involved till date in literature. Therefore, more detail investigations are still require to understand the mechanisms and reactions involved in heterogeneous catalytic decomposition of the  $\text{H}_2\text{O}_2$ . *In situ* spectroscopic techniques such as ATR-FTIR, EIS and DFT simulations and microscopy studies about the treated solution may be of good assistance in understanding the mechanisms and reactions involved in  $\text{H}_2\text{O}_2$  activation as well as those responsible for the transformation of the pollutants, thus allows adequate design of the electrochemical reactors and optimization of operating conditions. More importantly, there is need for pre-pilot, pilot and scale-up studies for Hetero-EF system with both catalysts and functionalized cathode material for treatment of synthetic and real effluents. Till date, all the studies reported in literature was performed on laboratory scale; as such full scale studies are required to understand the behavior of Hetero-EF system on large scale treatment reactors as well as optimization works with full cost and environmental impact. Besides, studies on flow reactors using either solid catalysts or functionalized cathode are very limited in literature, which implies that more studies are need to investigate feasibility of Hetero-EF system in flow reactors with aim of addressing the technical and economic perspectives.

## 8. Conclusion remarks

Heterogeneous electrochemical wastewater treatment system based on Fenton's chemistry is one of the most exciting and efficient emerging technologies for wastewater treatment owing to its applicability over wide pH widows and reusability of the catalysts in several runs. The desirable features for potential heterogeneous catalysts include high catalytic efficiency and stability over wide pH range, easy separation and reusability as well as environmental compatibility. The catalytic activation of  $\text{H}_2\text{O}_2$  to reactive oxygen species, especially  $\cdot\text{OH}$ , was by either homogeneous catalysis by dissolved  $\text{M}^{x+1}/\text{M}^x$  ( $\text{M}=\text{Fe}, \text{Cu}$  or  $\text{Co}$ ) redox couple or surface catalyzed process by surface metal species  $\equiv\text{M}^x-\text{OH}$  ( $\text{M}=\text{Fe}, \text{Cu}$  or  $\text{Co}$ ) and its one-electron reduzate ( $\equiv\text{M}^{x-1}-\text{OH}$ ) or both depending on the working pH at which the system operate and partly on the properties of the solid catalyst. Two known configurations of Hetero-EF and Hetero-PEF systems *vis-à-vis* solid catalysts (bare or supported iron/transition metal containing compounds) and Fe/Fe-compound functionalized cathodic materials were vividly examined. Relevant studies on Hetero-EF and Hetero-PEF approaches by using both solid catalysts and functionalized cathodic materials were summarized and it is safe to say that the latter is a more exciting treatment technique because of easy separation and reusability.

Catalytic fall-off, dissolution at strong acidic pH and agglomeration as well as multi-step/complex techniques for catalyst/functionalized cathode preparation are some of the major challenges encounter in Hetero-EF and Hetero-PEF treatments of organic pollutants. It can be anticipated that more studies and research groups will consider Hetero-systems in future due to its exciting features and logical growth in environmental concern and pollution remediation. Therefore future studies should be focused on improving the stability of the solid catalyst at acidic pH, investigating the use of Hetero-EF/PEF system on pilot scale and flow reactors and complete analysis of the economic and environmental impact of Hetero-EF treatment on biotic component of ecosystem as well as treatment of real wastewater.

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